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## Highlights

### **Ecosystem services and management of reed and seagrass debris on a urban Mediterranean beach (Poetto, Italy)**

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- A numerical approach assesses runup on a beach with seagrass wracks
- Large permeability values were measured in areas with seagrass and reed deposits
- Infiltration processes allow the beach to drain the overwashed water
- Reed and seagrass wracks can mitigate flooding by increasing beach permeability

# Ecosystem services and management of reed and seagrass debris on a urban Mediterranean beach (Poetto, Italy)

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## Abstract

This paper reports a scientific inquiry carried out within the management process of an exceptional accumulation of reeds and seagrasses that took place in December 2019 on Poetto beach (Cagliari, southern Sardinia, western Mediterranean). The magnitude of the event raised concern within the local community and tourism service providers especially for the compromised beach accessibility caused by this large amount of biomass. [The scientific inquiry is carried out in support of coastal management, to assess the berm processes before the removal of the reed wracks decided by the local municipality.](#) By means of a numerical approach, this work devotes special attention to the runup induced by storms in the presence of reed and seagrass deposits on a low-lying backshore. [Field surveys reported relatively large conductivity parameters in the presence on reed and seagrass deposits.](#) [The numerical approach shows that the increased beach permeability can eventually mitigate coastal flooding induced by storms.](#) These results highlight the ecosystem services provided by reed and seagrass wracks together with the implications for coastal protection and management.

*Keywords:* Coastal Flooding, Seagrass deposits, Ecosystem Services, Wave Modelling, Beach Resilience

*PACS:* 0000, 1111

*2000 MSC:* 0000, 1111

## 1. Introduction

Worldwide shorelines are often littered with biomass originating from terrestrial and marine ecosystems [1]. Regardless of its origin, this material is ultimately deposited on the backshore by waves under storm conditions. Recent work has addressed the role of woody debris in coastal processes such as dune evolution and growth [2, 3]. These studies have shown that dead trees and large logs (commonly referred to as driftwood) are a significant agent affecting morphodynamics of sandy beaches subject to appreciable aeolian sand transport. In fact, foredune development can benefit from the presence of woody debris that promote accumulation of windblown sand in the backshore. Moreover, Kennedy and Woods [4] suggest that woody debris act as a buffer to waves during storm events on gravel beaches.

*Posidonia oceanica* meadow is another source of biomass, along Mediterranean and southwestern Australian coastlines [5, 6], that storms uproot and transport from the shoreface, eventually accumulating it on the backshore [7]. The presence of seagrass necromass (leaves and rhizomes mixed with sand, commonly referred to as banquette or beach-cast litter) mitigates beach erosion induced by winter storms by promoting sediment retention and reducing sediment resuspension [8, 9].

The aforementioned work has contributed to the characterization of coastal processes induced by large woody debris and *Posidonia oceanica* banquettes, drawing attention to their ecosystem services. However, beside the services identified by the scientific community, the presence of this biomass often poses a management issue especially on beaches devoted to tourism. For instance, despite being a common feature on Mediterranean beaches, the *Posidonia oceanica* banquette is not always perceived positively by tourism service providers and beach-goers [10]. This has led local authorities to prepare guidelines devoted to the identification of strategies for the management of banquettes. Due to its recognized services offered in terms of coastal protection, in Italy the regulation of *Posidonia oceanica* falls within the exclusive competence of the state legislator. The regional legislative competence in the field of tourism can be exercised, only insofar as it is not in contrast with the state discipline. In Sardinia, the 2016 regional resolution (40/13 of 6.7.2016) entitled "Operational guidelines for the management of *Posidonia oceanica* deposits on beaches" suggests that the preferred management strategy is to keep the wracks on site. In the event that, for technical reasons that objectively hinder the usability of the beach in the summer season, keeping the

38 *Posidonia* deposits on site is extremely problematic, the option of moving  
39 and subsequent repositioning of the accumulations and the transfer to waste  
40 disposal or recovery plants can be pursued following some procedural and  
41 operating instructions.

42 Large woody debris and *Posidonia oceanica* wracks are not the only source  
43 of biomass on Mediterranean beaches. Small and medium-size woody debris,  
44 such as reeds proceeding from fluvial systems, are a common feature whose  
45 role in beach morphodynamics has received less attention by the scientific  
46 community [11]. In particular, to the best of the authors' knowledge, a quan-  
47 titative assessment of the role played by beach berms reinforced by seagrass  
48 and reed wracks on the protection of sandy beaches has not been reported.  
49 Moreover, probably due to the rarity of large reed deposition events, the  
50 management of these deposits is less regulated than the case of *Posidonia*  
51 *oceanica*. The absence of regulation leaves coastal managers without clear  
52 guidelines for the management of reed deposits on beaches.

53 This paper reports the scientific inquiry carried out within the manage-  
54 ment process of an exceptional accumulation of reeds (*Arundo donax* pro-  
55 ceeding from local fluvial systems) and seagrasses on the berm of Poetto  
56 beach (Cagliari, Southern Sardinia). Although reed deposition on Poetto  
57 beach is not unusual, an exceptional event occurred on December 2019 with  
58 a magnitude that had not been previously observed. The great amount  
59 of this biomass accumulated nearby the shoreline raised concerns especially  
60 among local tourism service providers, worried about its negative impacts.  
61 The municipality of Cagliari disposed the measures to bring the beach back  
62 to the previous state and, due to the absence of a legislation on the man-  
63 agement of reed deposits, commissioned the CMGG (Coastal and Marine  
64 Geomorphology Group) of the University of Cagliari to prepare a scientific  
65 inquiry, including the monitoring of the beach berm processes before, during  
66 and after the removal of reeds. The main purpose of the inquiry is thus to  
67 scientifically support and motivate the management decisions.

68 A special attention in the scientific inquiry is devoted to runup and flood-  
69 ing on Poetto beach, characterized by low-lying sandy backshore and the  
70 implications for coastal protection and management. The shape of Poetto  
71 beach profile, with a berm higher than a large portion of the emerged beach,  
72 allows to consider the implications of using vertical and horizontal runup  
73 values in the assessment of beach flooding. The runup assessment conducted  
74 through a numerical approach benefited from the preparatory field work, in-  
75 cluding beach surveys and permeability tests. Beach surveys reported large

76 spatial variability of hydraulic conductivity across the beach, related to the  
77 distribution of reed and seagrass deposits within the sediment. The role  
78 of infiltration/exfiltration processes on a low-lying sandy beach under over-  
79 wash events is investigated in detail. For this purpose, we identified the  
80 major storms that hit the study area during the monitoring period to assess  
81 the storm-induced coastal flooding through numerical modelling including  
82 groundwater flow processes.

83 The paper is structured as follows. Sections 2 and 3 introduce the geo-  
84 graphical settings together with the event which drove the reed deposition  
85 on the beach berm. Section 4 describes the monitoring program along with  
86 the numerical approach. Section 5 reports the results from the hydrody-  
87 namic modelling. Section 6 discusses the results and Section 7 draws some  
88 conclusions.

## 89 2. Geographical settings

90 Poetto beach lies in the innermost part of the Gulf of Cagliari, South-  
91 ern Sardinia (Italy), inside the metropolitan area of Cagliari (Figure 1). It  
92 is a micro-tidal urban sandy beach with a length of 8 km and a maximum  
93 width of about 100 m. The beach is backed by a relatively narrow primary  
94 dune system (foredunes and embryo dunes) bordered by a residential neigh-  
95 borhood and a 4-lane motorway that connects the two main towns of the  
96 metropolitan area: Cagliari and Quartu Sant'Elena. Moreover, from the ad-  
97 ministrative point of view, the beach is divided into two sectors of similar  
98 size: the municipality of Cagliari manages the western sector whereas Quartu  
99 Sant'Elena manages the eastern part. A nourishment project carried out in  
100 2002 in the Cagliari municipality sector has significantly modified the tex-  
101 tural, compositional and morphological features of the backshore, shoreline  
102 and shoreface [12]. Besides, an increasing anthropic pressure, mainly related  
103 to the touristic sector, is responsible for an impact on the beach system,  
104 significantly affecting morphodynamic processes [13].

105 Wave conditions along Poetto beach system result from a combination  
106 of Mediterranean swells and locally-generated wind waves, with directions  
107 mainly ranging from South-East to South-South-West, see the wave rose in  
108 Figure 1. The Copernicus Marine Environment Monitoring Service (CMEMS)  
109 database covering the period 2006-2018 gives a mean significant wave height  
110  $H_s$  of 0.4 m at the virtual buoy in front of the beach. Scirocco storm events  
111 drive the most intense swells that hit the beach from South-East and South-

112 South-East directions. Moreover, the South-South-West sector contains con-  
 113 siderable wave energy that is mainly related to West-South-West swells that  
 114 enter the Gulf of Cagliari. Under these conditions, the wave direction in front  
 115 of Poetto beach is the result of the shelter offered by Capo Spartivento (the  
 116 Southernmost promontory of Sardinia) and wave refraction in the nearshore.  
 117 The emerged beach of Poetto is periodically flooded by South-East storms,  
 118 with a flooding extension that episodically can reach the coastal street and  
 119 nearby proprieties [12].

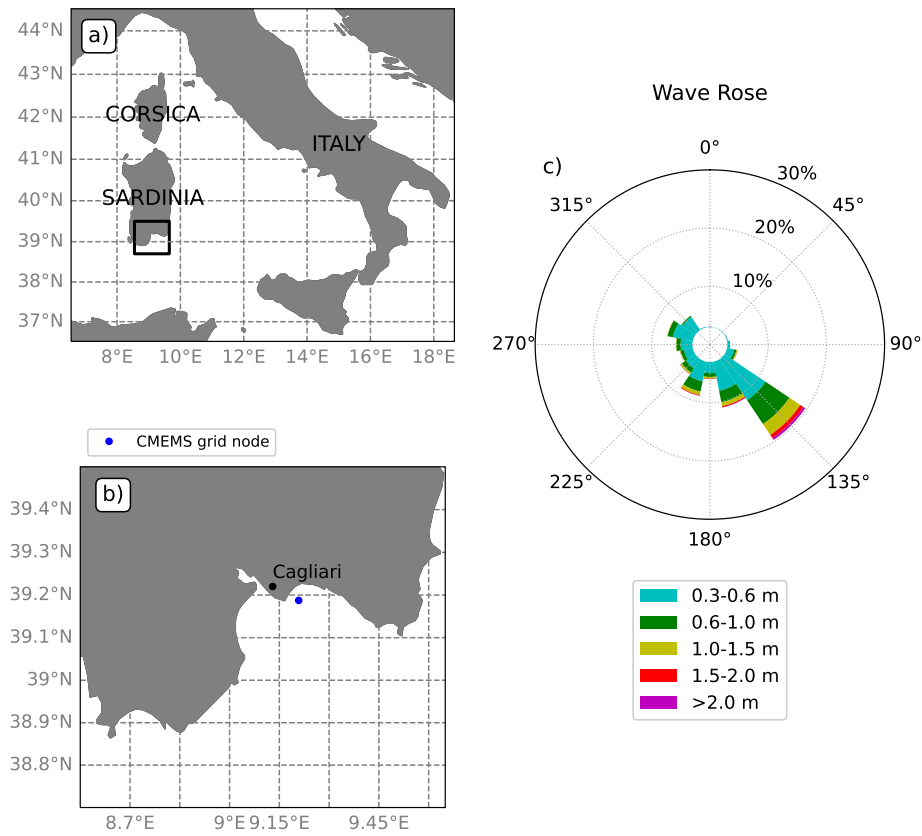


Figure 1: a) and b) Geographical settings with the location of the virtual buoy in front of the Poetto beach indicated by the blue dot in panel b). c) Wave rose at the virtual buoy from the CMEMS database (2006-2018).

120 **3. Event analysis**

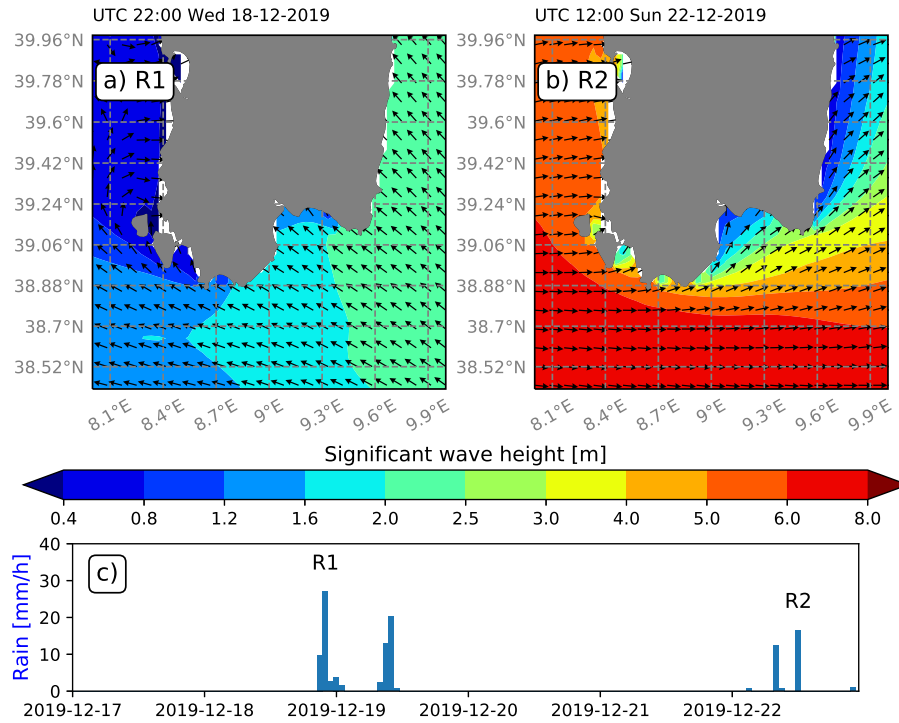


Figure 2: a) and b) Significant wave height during the two events R1 and R2 that drove the reed deposition and redistribution along the Poetto beach (Wave data from the CMEMS database). c) Precipitation rate measured at the Poetto beach.

121 Heavy rain precipitation events occurred between the 18/12/2019 and the  
 122 22/12/2019 in the metropolitan area of Cagliari. The meteorological station  
 123 located on the roof of a building in close proximity to the Poetto beach  
 124 recorded precipitation peaks above 25 mm/h between 18:00h and 24:00h of  
 125 the 18/12/2019 (the average yearly total precipitation is on the order of 500  
 126 mm in Cagliari). This weather events triggered a rapid increase of runoff  
 127 discharged by surface streams to the Gulf of Cagliari. The resulting flows  
 128 were able to put in motion and transport to the sea a considerable amount  
 129 of biomass. The upper panels of Figure 2 displays the wave propagation in  
 130 the Gulf of Cagliari at the moment of the two rain peaks indicated as R1  
 131 and R2 in the lower plot.



132 Once it reached the sea, this biomass, made mostly up of uprooted reeds  
133 (*Arundo donax*) from local streams, was transported and spread by marine  
134 currents and waves driven by the energetic South-East swell that battered  
135 Southern Sardinia coasts during these days. Figure 2a shows that the signif-  
136 icant wave height was above 1.5 m in the nearshore of the Gulf of Cagliari.  
137 Few days later the event that triggered the reed transport to the sea, a mas-  
138 sive South-West storm approached the southern Sardinian coasts. Significant  
139 wave heights of above 6 m were expected on the western coasts of the islands  
140 of San Pietro and Sant’Antioco. This massive swell, although attenuated by  
141 the shelter offered by Capo Spartivento (the southernmost Sardinian land),  
142 entered the Gulf of Cagliari and played a role in the redistribution of reeds  
143 along the shore, see Figure 3a. Figure 2c shows the evolution of the rain rate  
144 during the third week of December 2019, together with the significant wave  
145 height maps during the two rain rate peaks identified as R1 and R2 in the  
146 figure. The precipitation was measured by a meteorological station managed  
147 by the CMGG, located on the roof of a hospital immediately behind Poetto  
148 beach. Wave data proceed from the CMEMS database that uses the spectral  
149 wave model WAM to simulate the wave evolution with a spatial resolution  
150 of  $1/25^\circ$  of latitude and a time resolution of 1 hour.

151 The great amount of biomass accumulated on the shoreline raised con-  
152 cerns especially among local tourism service providers, worried about its  
153 negative impacts in terms of beach accessibility. Due to the absence of leg-  
154 islation and the strategic importance of the beach for the local community,  
155 the municipality of Cagliari involved stakeholders, the University and local  
156 authorities in the decision making process with the objective of identifying  
157 a shared strategy about the management of this exceptional event. Once  
158 the options of 1) keeping the deposits on site and 2) their temporal move-  
159 ment have been considered as not viable options, the municipality of Cagliari  
160 disposed the measures to remove the reed deposits from the beach and com-  
161 missioned the CMGG group of the University of Cagliari for the monitoring  
162 of the beach berm processes. Following the suggestion made by the CMGG  
163 and in agreement with the guidelines listed by the Sardinian legislation for  
164 the *Posidonia oceanica* management, the municipality disposed that the re-  
165 moval operations of reed berms should have been carried out in a sustainable  
166 way, preserving the natural characteristics of the beach. In fact, the reeds  
167 were removed manually (see Figure 3b) avoiding the use of heavy machinery  
168 that usually causes a considerable loss of sediments, resulting in changes in  
169 the beach morphology (e.g., flattening of the beach profile, sediment com-

170 pacting and obliteration of sedimentary features like berms, beach-face steps,  
171 etc).

172 The management of this local exceptional event was affected by a larger  
173 global exceptional event: the corona virus (COVID-19) emergency. To con-  
174 tain the emergency, in March 2020 the Italian government imposed a national  
175 lockdown with strong restrictions on economic activities and the closure of  
176 beaches to public access. The lockdown lasted until May 2020 and under this  
177 period scientists had the unprecedented opportunity to observe ecosystem dy-  
178 namics with almost no human interference. The beach berm reinforced by  
179 the presence of reeds stayed in place until its removal that occurred in April  
180 and May 2020.

## 181 4. Methods

### 182 4.1. Monitoring program

183 The monitoring of the eco-geomorphological dynamics at Poetto beach  
184 included actions before and after the reeds removal: topographic and bathy-  
185 metric surveys, collection of the rectified images through the videomonitor-  
186 ing system and permeability tests. This section describes only the topo-  
187 graphic/bathymetric surveys and the permeability tests.

188 The topographical surveys were carried out along two transects in the  
189 western sector of the beach. Data were collected using DGPS in a GNSS  
190 (Global Navigation Satellite System) at frequency of 1 Hz. The transects  
191 run over the emerged beach from the dune system to the shallow shoreface at  
192 about one meter depth. The shoreface bathymetry along each transect was  
193 recorded using a single-beam echo-sounder coupled with a DGPS receiver  
194 interacting with a navigation software (frequency of 5 Hz). The topographic  
195 and bathymetric data were combined to obtain a morphological profile of the  
196 emerged and submerged beach, from the dune system up to the upper limit  
197 of the *Posidonia oceanica* meadow (depths 10-15 m at Poetto). Figure 4  
198 shows the beach profiles surveyed along the two transects T3 and T7 before  
199 the removal of the reeds. In Figure 4c it is also possible to identify the upper  
200 limit of the *Posidonia oceanica* meadow that lies where the profile becomes  
201 noisy due to the presence of seagrass below 8/10 m depth for transects T7.

202 Infiltrometric tests conducted with double-ring infiltrimeters allowed the  
203 characterization of the hydraulic conductivity on the sandy beach and on the  
204 beach berm with banquette. The permeability coefficients on sand ranged  
205 between 0.00003 m/s on the backshore and 0.0003 m/s on the beach berm



Figure 3: a) Reed accumulation on the berm of Poetto beach. b) Removal operations of reed deposits.

206 with buried reeds. Larger permeability coefficients were measured on the  
 207 beach berm with seagrass litter: they ranged between 0.14 and 0.15 m/s.

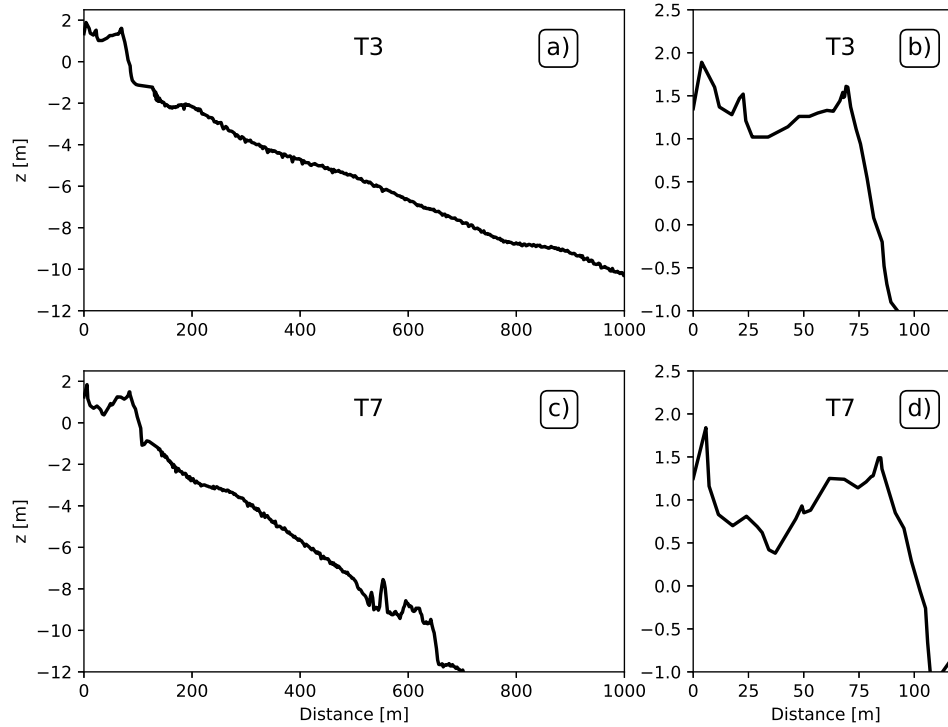


Figure 4: a) and c) Beach profiles along the two transects T3 and T7. b) and d) Details of the foreshore and emerged beach profiles.

#### 208 4.2. Storm identification

209 Incoming wave conditions at Poetto beach, for the period comprised be-  
 210 tween the deposition of reeds in December 2019 and their complete removal  
 211 in May 2020, were collected from the CMEMS hindcast time series [14]. For  
 212 this purpose we chose the grid node of the computational domain located in  
 213 front of Poetto beach. Figure 1b shows the location of the CMEMS system  
 214 grid node indicated as virtual buoy, whereas Figure 5 plots the time series  
 215 of the incident wave parameters at that location: significant wave height

216 ( $H_s$ ), mean period ( $T_m$ ) and mean direction ( $\theta$ ). Panel d) of Figure 5 shows  
217 the mean sea level ( $m_{sl}$ ) evolution recorded by the tide gauge located inside  
218 the Cagliari harbour, 4 km away from the Poetto beach. The analysis of  
219 the evolution of the significant wave height highlights several storms, among  
220 which it is possible the identification of the two storms that drove the reed  
221 deposition and their following redistribution along the Poetto beach in the  
222 month of December 2019. The most intense storm in the observation period  
223 occurred from the 20th to the 23th of January 2020 (with a peak on the  
224 evening of the 21st of January with significant wave heights of 2.9 m).

225 We used the peak-over-threshold (POT) [15] method to identify the 48-  
226 h independent storms occurred during the observation period at the vir-  
227 tual buoy location represented by the CMEMS grid node. We identified the  
228 storms based on the prominence parameter for the significant wave height  
229  $H_s$ : the prominence threshold was chosen equal to 0.6 m. Although the  
230 threshold value of 0.6 m may seem low for extreme event analysis, due to the  
231 moderate incoming wave energy levels at Poetto (mean  $H_s$  is 0.4 m), this  
232 method allowed the identification of 12 storms during the five-month period  
233 considered. We retained only the storms with a persistence above the thresh-  
234 old longer than 6 h, that met the independence criterion with more than 48 h  
235 between the peak of a storm and the peak of the following one. The extreme  
236 wave parameters representative of each storm of the sample were selected  
237 as the values occurring at the time in which the maximum wave height was  
238 observed during the storm duration. Table 1 reports the dates of occurrence  
239 together with the wave parameters and the mean sea level of the identified  
240 12 storms. The last column of the table lists the effects observed from the  
241 video monitoring system.

### 242 *4.3. Modelling approaches*

#### 243 *4.3.1. Phase-averaged modelling*

244 To evaluate the role played by the organic berm in coastal protection from  
245 flooding, the incident wave conditions collected at the nearshore grid nodes  
246 of the CMEMS system were numerically propagated in the nearshore with  
247 the SWAN model [16]. The SWAN model is a spectral wave model based  
248 on the wave action equation. It is nowadays widely used to address wave  
249 nearshore processes [17, 18]. The wave spectra reconstructed at six nodes of  
250 the CMEMS system represented the wave conditions imposed at the bound-  
251 ary of the numerical grid used for the wave propagation with SWAN (Figure  
252 6). The six grid nodes lie along the open SWAN boundaries at West, South

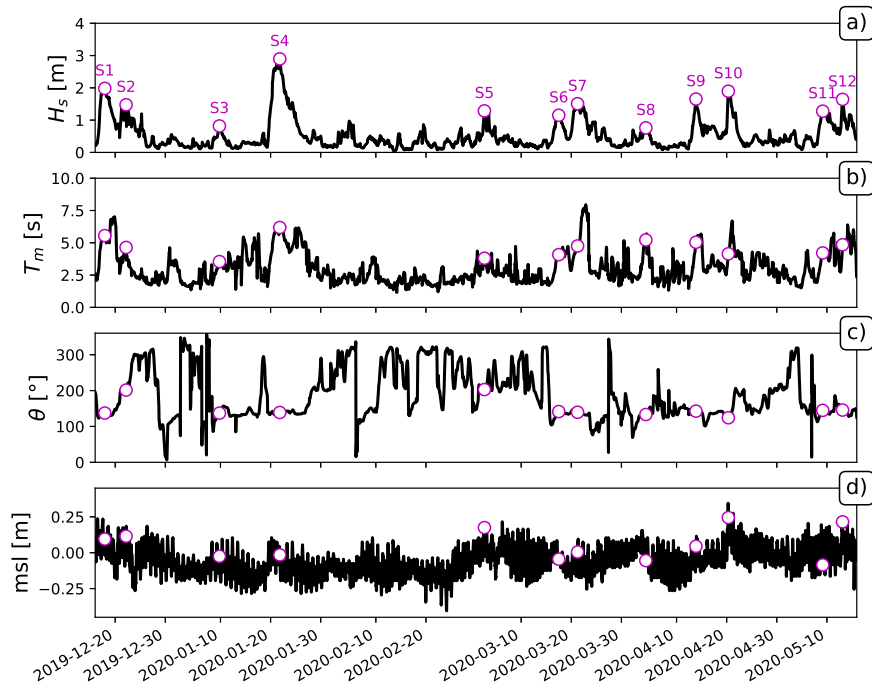


Figure 5: Time series of wave parameters and mean sea level at the Poetto beach during the observation period. a) Significant wave height, b) mean period, c) mean wave direction, d) mean sea level. The circles highlights the main storm events.

253 and Est of the grid. The spectral reconstruction routine was necessary since  
 254 CMEMS does not provide the full frequency-directional spectra but it makes  
 255 available the partition parameters ( $H_s, T_m$  and  $\theta$ ) for two swells and one wind  
 256 sea component. The partition parameters from CMEMS were used to reconstruct  
 257 the full spectra at the boundary nodes. For this purpose we inferred  
 258 the full frequency-directional spectrum as a sum of the three partitioned spectra  
 259 (primary and secondary swell and wind wave component) reconstructed  
 260 from the partition parameters, assigning a parametric spectral shape (JON-  
 261 SWAP) with a large directional spread to the wind wave component with  
 262 respect to the swell components. The routine of spectrum reconstruction at

Storm	Date	Hour	$H_s$ [m]	$T_p$ [s]	$T_m$ [s]	Dir [o]	mssl [m]	Effects
S1	2019-12-17	22:00	1.98	8.39	5.56	137.30	0.09	overwash
S2	2019-12-22	04:00	1.48	11.17	4.64	201.35	0.11	none
S3	2020-01-09	19:00	0.82	5.73	3.54	137.14	-0.02	none
S4	2020-01-21	20:00	2.90	8.39	6.18	138.90	-0.02	overwash
S5	2020-03-02	16:00	1.29	5.73	3.80	202.74	0.17	none
S6	2020-03-17	12:00	1.15	6.93	4.08	141.53	-0.05	none
S7	2020-03-21	06:00	1.51	7.63	4.76	139.53	0.01	none
S8	2020-04-03	21:00	0.76	8.39	5.22	133.24	-0.05	none
S9	2020-04-13	21:00	1.65	6.93	5.04	142.70	0.04	none
S10	2020-04-20	08:00	1.90	7.63	4.15	124.24	0.24	overwash
S11	2020-05-09	04:00	1.28	6.30	4.22	144.79	-0.09	none
S12	2020-05-13	03:00	1.64	6.93	4.85	145.67	0.21	none

Table 1: Wave parameters and mean sea level during the storms occurred in the period December 2019-May 2020 at Poetto beach. The last column lists the effects observed from the video monitoring system.

263 each node can be summarized as follows:

- 264 • reconstruction of the frequency-directional spectrum with JONSWAP  
265 shape ( $\gamma=3.3$ ) and directional spread of  $19^\circ$  from the bulk wave param-  
266 eters of the primary swell partition provided by CMEMS
- 267 • reconstruction of the frequency-directional spectrum with JONSWAP  
268 shape ( $\gamma=3.3$ ) and directional spread of  $19^\circ$  from the bulk wave param-  
269 eters of the secondary swell partition provided by CMEMS
- 270 • reconstruction of the frequency-directional spectrum with JONSWAP  
271 shape ( $\gamma=3.3$ ) and directional spread of  $25^\circ$  from the bulk wave param-  
272 eters of the wind-wave partition provided by CMEMS
- 273 • the total spectrum is the sum of the three previous spectra

274 This routine with the spectrum reconstruction from wave spectral partitions  
275 represents an improvement with respect to the reconstruction from total bulk  
276 wave parameters (adopted, for instance, by [17]) since it allows the charac-  
277 terization of multi-modal seas. Figure 7 shows the result of the spectral  
278 reconstruction routine for storm S12. From the comparison of panels a) and  
279 c) it is possible to appreciate the different shapes of the swell and the wind

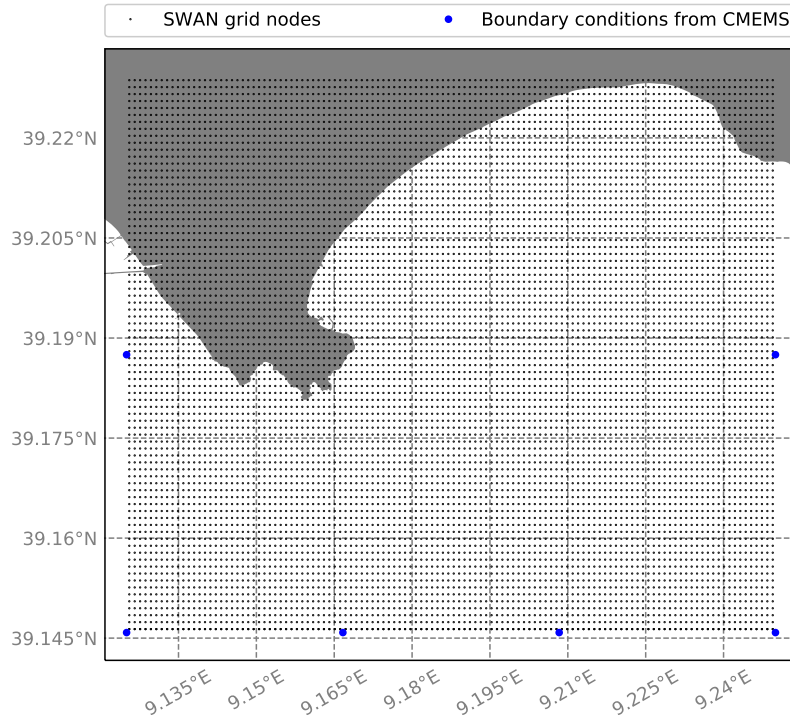


Figure 6: Computational grid domain in SWAN. The blue points are the CMEMS grid nodes in which the boundary conditions for SWAN are reconstructed.

280 wave spectra with the latter characterized by a larger directional spread.  
 281 Panel b) suggests that for storm S12 the secondary swell virtually carry no  
 282 energy, which is a common situation in a closed basin as it is the Mediter-  
 283 ranean Sea. As a result, the total spectrum for storm S12 is simply given by  
 284 the sum of the primary swell (the secondary swell is close to zero) and the  
 285 wind wave spectra.

286 The grid used in the SWAN simulation (Figure 6) has a spatial resolution  
 287 of 1/16 of nautical mile (about 115 m) and allows the achievement of the  
 288 wave conditions in the proximity of Poetto beach and the identification of  
 289 the main wave transformation processes in coastal water.

290 The reliability of the spectral wave modelling approach is assessed by compar-  
 291 ing the SWAN output with wave measurements in coastal water. Since  
 292 we do not have measurements available in the observation period, we use the  
 293 data collected by an AWAC (Acoustic Wave And Current) profiler deployed



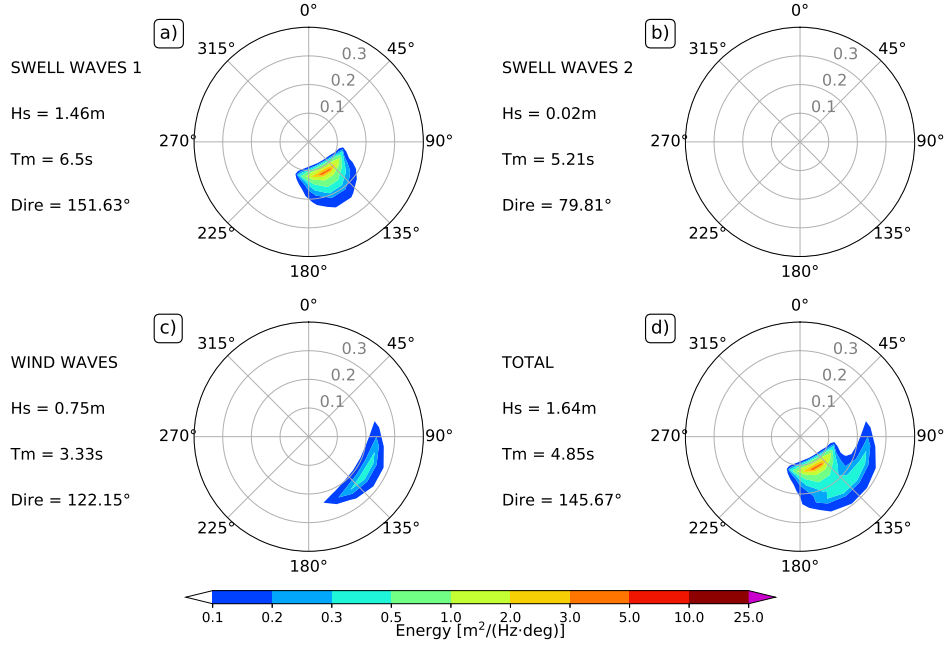


Figure 7: Reconstruction of spectral wave boundary conditions (storm S12) from bulk swell and wind wave parameters. a) Primary swell wave spectrum, b) secondary swell wave spectrum, c) wind wave spectrum, d) total wave spectrum.

294 in the nearshore of Poetto at a water depth of 18 m during two field cam-  
 295 paigns conducted, respectively, in Spring 2017 and Fall 2020. Further details  
 296 about the field campaign and the exact AWAC location can be found in Ruju  
 297 et al. [19]. The adoption of the procedure described in section 4.2 allows the  
 298 identification of 5 wave events, whose  $H_s$  is between 0.9 and 2.8 m. These  
 299 events are simulated with SWAN following the routine described in section  
 300 4.3.1. Here, we adopt the normalized root-mean-square-error  $NRMSE$ ,  
 301 defined as follows:

$$NRMSE = \sqrt{\frac{\sum (O_i - M_i)^2}{\sum O_i^2}}, \quad (1)$$

302 where  $O_i$  and  $M_i$  are the observed and modelled variables. The NRMSE  
 303 of  $H_s$  is equal to 0.137. This value of NRMSE is consistent with the error  
 304 metrics range reported by recent studies dealing with spectral wave modelling  
 305 in coastal water [14, 17], thus proving the ability of the adopted approach in  
 306 modelling nearshore wave dynamics.

307 *4.3.2. Phase-resolving modelling*

308 The spectra obtained as output of the SWAN simulations were used as a  
309 boundary conditions for the wave-resolving model XBeach [20] covering the  
310 shallow water area. The nonhydrostatic module of XBeach used in this study  
311 is based on the nonlinear shallow water equations, including a nonhydrostatic  
312 term to account for frequency dispersion in intermediate water. Simulations  
313 were setup in 1D cross-shore mode along the two transects T3 and T7, see  
314 Figure 8. The numerical domain covered the nearshore area from 14 m of  
315 depth up to the toe of the dune system. The seaward boundary with a water  
316 depth of 14 m was chosen since it lies in proximity of the outward boundary  
317 of surf zone of major storms at Poetto. The choice of the offshore water  
318 depth for the 1D XBeach simulations follows from a compromise between  
319 two considerations. On one hand it is desirable to have the boundary as  
320 close as possible to the shore so that the wave field includes the effects of  
321 the refraction processes caught by SWAN. On the other hand, a boundary  
322 placed in water too shallow would lead to strong nonlinearities with a large  
323 and unrealistic second-order long-wave generation. See also the recent work  
324 of Fiedler et al. [21] addressing the role offshore boundary conditions in surf  
325 zone modeling.

326 The mean water level of each XBeach simulation was set according to  
327 the level measured by the tidal gauge. To provide a detailed description of  
328 swash zone processes, the horizontal spatial grid resolution increased shore-  
329 ward from 3.5 m in the generation zone up to 0.5 m in the swash zone,  
330 see Figure 9. The offshore boundary generated the time series of incoming  
331 waves from the SWAN spectrum and absorbed the outgoing waves resulting  
332 from beach reflection. The model accounted for friction through the Chezy  
333 coefficient setup to  $30 \text{ m}^{0.5}/\text{s}$ , which is consistent with previously reported  
334 constant friction coefficients of 0.015 [22]. Infiltration/exfiltration processes  
335 were simulated by including a constant permeability coefficient of 0.0003  
336  $\text{m}/\text{s}$ , equal to that measured on the beach berm in presence of reeds. We  
337 identify the runup toe as the shoreward point with water depth larger than  
338 0.05 m.

339 To assess the role played by the reed-reinforced berm in coastal protection,  
340 we calculate the storm-induced runup both with an empirical approach and  
341 with XBeach modelling. We focus on the aforementioned 12 storms occurred  
342 in the period of observation. The total water level  $TWL$  is calculated as:

$$TWL = MSL + R_{2\%}, \quad (2)$$

343 in which  $MSL$  is the mean sea level and  $R_{2\%}$  is the 2% exceedence level for  
 344 runup.  $MSL$  is obtained from the tide gauge installed inside the Cagliari  
 345 harbour.

346 In the empirical approach, the runup contribution to the flooding level  
 347 is determined from the spectral wave parameters ( $H_S$  and  $T_p$ ) computed by  
 348 SWAN along the two transects T3 and T7 at a water depth of 14 m. The  
 349 runup contribution to the flooding elevation is then obtained through:

$$R_{2\%} = 1.1(\langle\eta\rangle + \frac{S}{2}), \quad (3)$$

350 where  $\langle\eta\rangle$  is the wave setup and  $S$  is the significant swash. Here,  $\langle\eta\rangle$  and  $S$   
 351 are estimated from  $H_S$ ,  $T_p$  and the foreshore slope  $\beta$  according to Stockdon  
 352 et al. [23].

$$R_{2\%} = 1.1(0.35\tan\beta(H_0L_0)^{1/2} + \frac{[H_0L_0(0.563\tan\beta^2 + 0.004)]}{2}) \text{ for } \xi_0 \geq 0.3, \quad (4)$$

353 and

$$R_{2\%} = 0.043(H_0L_0)^{1/2} \text{ for } \xi_0 < 0.3, \quad (5)$$

354 where  $H_0$  and  $L_0$  are the deep-water significant wave height and wavelength.  
 355  $\xi_0$  is the Iribarren number or surf similarity parameter, computed as:

$$\xi_0 = \frac{\tan\beta}{(H_0L_0)^{1/2}}. \quad (6)$$

356 In the numerical approach based on XBeach,  $R_{2\%}$  is obtained directly from  
 357 the computed runup time series.

## 358 5. Results

359 The  $TWL$  values from the empirical and numerical approaches are com-  
 360 pared in Figure 10.  $TWL$  calculated with the empirical method and  $TWL$   
 361 from XBeach are in good agreement. Since both approaches include the same  
 362  $MSL$  (from the tidal gauge), they can only differ as a result of the runup  
 363 parameter  $R_{2\%}$ . This agreement highlights the general reliability of these dif-  
 364 ferent methods for runup and flooding calculations. Considering the XBeach  
 365 output as reference value, the NRMSE of the  $TWL$  is equal to 0.235 and  
 366 0.179 for transects T3 and T7, respectively. Moreover, Figure 10 is in good

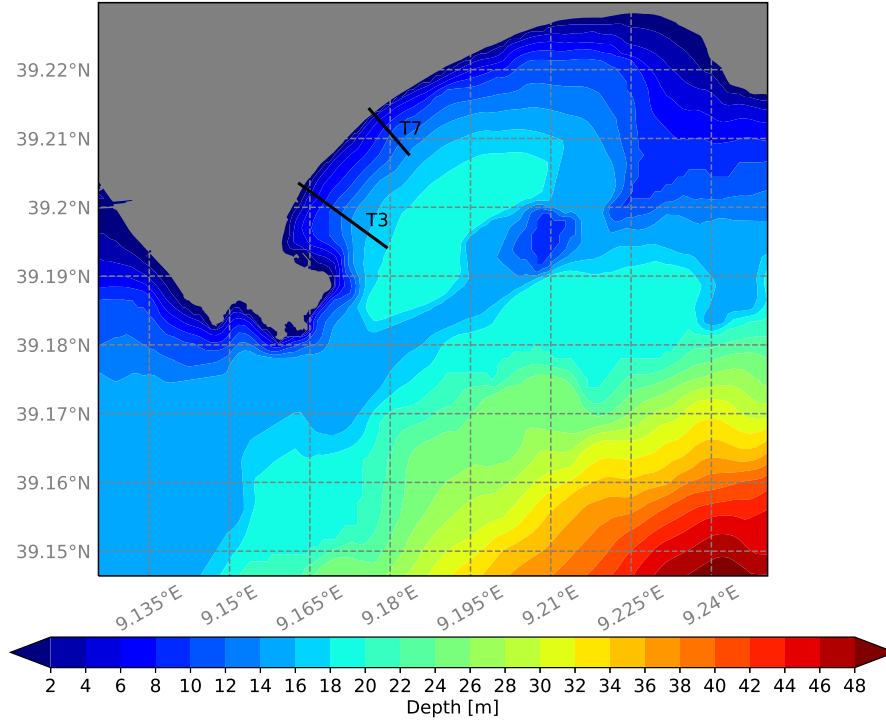


Figure 8: Detail of the bathymetry in the Gulf of Cagliari with the transects T3 and T7.

367 agreement with visual observations obtained from the video camera system.  
 368 In fact, the images captured from the video camera revealed significant berm  
 369 overwash during the S1 and S4; whereas storms S10 and S12 led to isolated  
 370 overwash events. These four storms are identified as those driving the highest  
 371  $TWL$  values at the two transects at Poetto beach.

372 Figure 11 shows the horizontal total water distance  $TWD$  from XBeach  
 373 simulations. Both the  $TWL$  and the  $TWD$  include the  $R_{2\%}$  parameter com-  
 374 puted as the 2% exceedence level from the XBeach runoff time series.  $TWL$   
 375 takes into account the vertical runoff, whereas the horizontal runoff con-  
 376 tributes to  $TWD$ . The  $TWD$  parameter gives an insight of the flooding  
 377 magnitude that is more difficult to achieve from the vertical  $TWL$ . This is  
 378 mainly due to the fact that large part of the emerged beach lies below the  
 379 berm elevation. In fact, sea conditions leading to overwash such as S1 and  
 380 S4 give a  $TWL$  only few cm above the berm height, whereas the  $TWD$  is  
 381 few meters beyond the berm crest location, indicated by the dashed line in

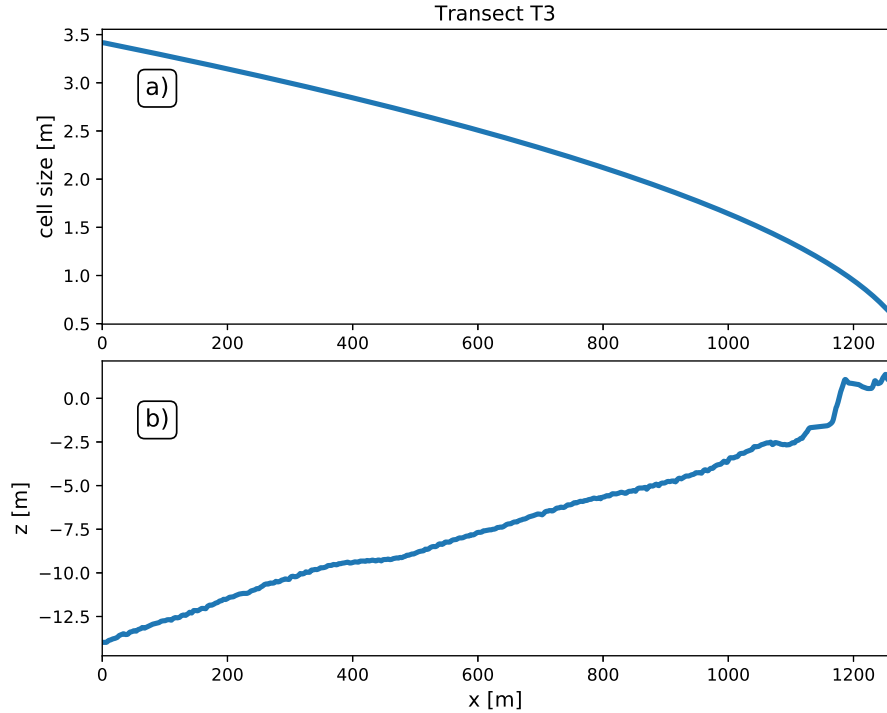


Figure 9: a) Grid size variation across the XBeach computational domain for transect T3. b) Beach profile along T3.

382 Figure 11. Figure 11 is consistent with Figure 10 allowing the identification  
 383 of the four storms driving berm overwash. In addition, Figure 11 reveals the  
 384 difference in flooding magnitude between the most severe storm S4 and the  
 385 less strong storms S10 and S12.

386 Figure 12 displays the time series of swash dynamics during storm S1,  
 387 providing details of overwash dynamics on a low-lying backshore. Panel c)  
 388 shows that vertical runup does not significantly overcome the berm elevation,  
 389 although major uprushes are able to drive overwash. Instead, the horizontal  
 390 runup time series (Figure 12d) allows the identification of uprush events  
 391 leading to overwash in which the berm crest location is exceeded. The upper  
 392 panel highlights how effectively the infiltration processes drain the volume of  
 393 water that overwashes the berm. In the simulation of the storm S1, the water  
 394 accumulated by an overwash event over the emerged beach is completely  
 395 drained before the arrival of the next overwash.

396 To investigate the importance of infiltration processes, we conducted an-  
397 other set of XBeach simulations using the hydraulic conductivity measured  
398 on the backshore on the sandy substrate, without the presence of buried  
399 reeds. Figure 13 compares the computed flooding induced by the identified  
400 storms on the profile with a permeability coefficient of  $0.00003 \text{ m/s}$  with  
401 that computed on the profile with a permeability coefficient of  $0.0003 \text{ m/s}$ .  
402 In other words, the XBeach boundary conditions were the same in the two  
403 configurations that differed only in the hydraulic conductivity. To prevent  
404 the possible variability linked to wave groupiness [24], not only the spectral  
405 shape but also the time series of the boundary conditions were conserved.  
406 In general terms, under the same environmental forcing, a lower hydraulic  
407 conductivity seems to increase the flooding extension under overwash condi-  
408 tions. The strongest TWD increases are found in run S4 on transect T3 (13  
409 m) and in run S1 on transect T7 (7 m). On the other hand, under moderate  
410 wave conditions without overwash, infiltration processes have no significant  
411 effect of runup and TWD values.

412 The assessment of beach flooding through a numerical approach shows  
413 that four storms (S1, S4, S10 and S12) drove berm overwash during the ob-  
414 servation period. Storms S1 and S4 led to significant overwash and flooding,  
415 whereas storms S10 and S12 produced only isolated overwash events with  
416 limited beach flooding. These results confirm the analysis of the images ob-  
417 tained from the video-monitoring system (the video-monitoring system did  
418 not detect overwash under storm S12 probably because this event happened  
419 at night and the moderate overwash left no visible marks on the beach). Un-  
420 der energetic conditions, once the berm is overwashed, the relative depression  
421 in the beach geometry favours the beach flooding towards the dune system.  
422 Numerical simulations conducted with different hydraulic conductivity coeffi-  
423 cients allow the assessment of the role played by beach permeability on runup  
424 and flooding. According to previous studies [25] suggesting that on sandy  
425 beaches weak infiltration processes are not able to modify swash dynamics,  
426 no appreciable differences in runup are found for moderate wave conditions  
427 in which the swash zone does not exceed the berm crest. Nevertheless, the  
428 results suggest that a low permeability coefficient tends to increase flood-  
429 ing under severe forcing leading to overwash. This process can be observed  
430 in Figure 14 showing the comparison of two snapshots taken at the same  
431 moment in which a wave is overwashing the berm from the XBeach simula-  
432 tions of storm S1. The difference in permeability does not yield appreciable  
433 changes in the runup location (indicated by the red dot) in proximity of the

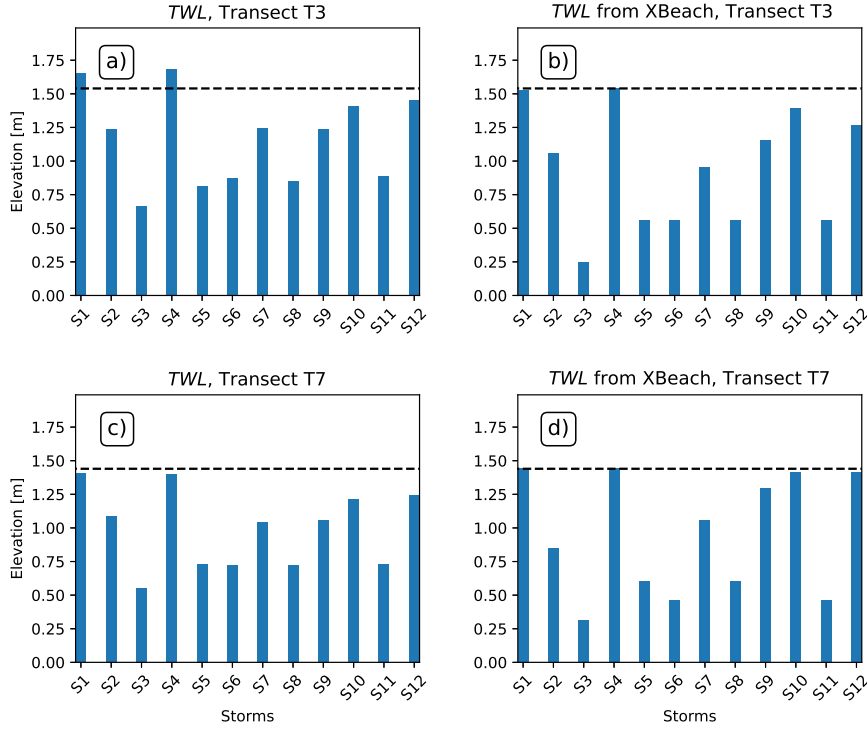


Figure 10: Total water level  $TWL$  using parametric formulas for runup (a and c) and from XBeach simulations (b and d). The dashed line is the beach berm height above mean sea level.

434 berm. At the same time, the panel c) of the figure highlights how the low  
 435 permeability precludes a complete evacuation of the water from the emerged  
 436 beach. The water that overwashes the berm tends to accumulate on the  
 437 emerged beach, eventually increasing the flooding area.

438 The simulations carried out so far have considered a homogeneous friction  
 439 factor (Chezy equal to  $30 \text{ m}^{0.5}/\text{s}$ ) over the entire beach profile. However, it  
 440 is plausible that seagrass and reed deposits can enhance friction dissipation  
 441 by increasing roughness at the bed. To quantify possible implications for  
 442 coastal flooding, we have run a new set of simulations in which the friction  
 443 was increased in the region of the profile covered with wracks over the T3  
 444 profile (we did not consider T7 since it is not in the area monitored from  
 445 the video camera system). On the day in which the topographic survey was  
 446 conducted, the videocamera system showed seagrass and reed wracks deposits

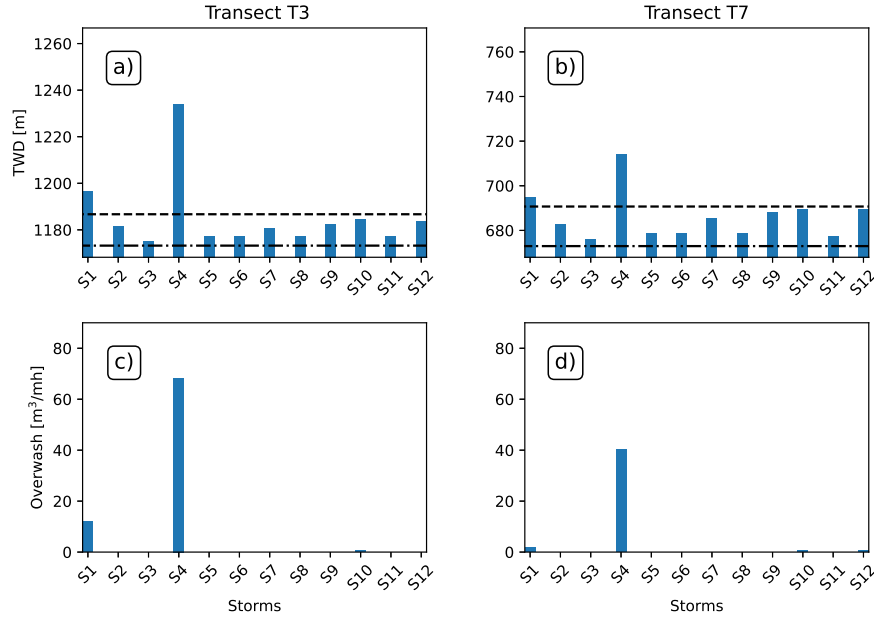


Figure 11: a) and b) Horizontal total water distance from XBeach simulations. The dashed line and the dot-dashed line are the cross-shore location of the beach berm crest and the mean water level, respectively. c) and d) Overwash rate

447 that extended over 5 m landward from the berm of the profile of transect  
 448 T3. The Chezy friction coefficient was set to  $10 \text{ m}^{0.5}/\text{s}$  over this area, a value  
 449 chosen according to Chow [26] (vegetal lining). The permeability and other  
 450 parameters were kept constant as in the previous simulations. Whereas the  
 451 TWD induced by the most energetic storm S4 is not affected by the change in  
 452 friction, a slightly reduction of 1 m is observed only for run S1 (not shown).  
 453 This may be related to the flooding extension whose landward limit falls in  
 454 proximity of the wracks in run S1. As expected, the locally-increased friction  
 455 does not yield any TWD change under moderate storm conditions in which  
 456 no overwash occurs.

## 457 6. Discussion

458 The approach followed in this work allows the assessment of runup and  
 459 flooding on a low-lying backshore following an exceptional event of reed  
 460 (*Arundo donax*) deposition. Particular attention is devoted to the overwash



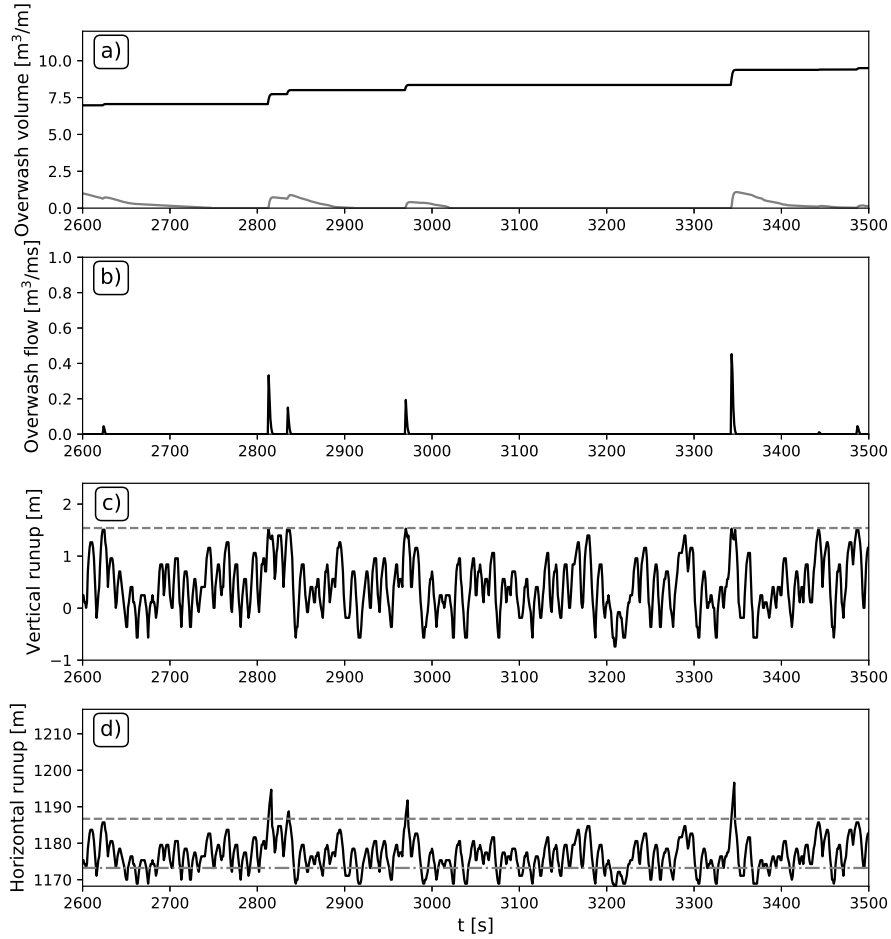


Figure 12: Time series of swash dynamics. a) The black line is the cumulative overwash volume; the gray line is the water volume accumulated over the emerged beach. b) Instantaneous overwash flow. c) Vertical runup. The dashed line is the berm crest elevation. d) Horizontal runup. The dashed line is the berm crest location, whereas the dot-dashed line is the intersection between the mean water level and the beach profile.

461 dynamics over the berm and to the infiltration processes occurring on the  
 462 emerged beach. This section discusses [the implications](#) of the results together  
 463 with the limitations and assumptions related to the adopted methodology.

464 We estimate the runup and flooding at Poetto beach through a model  
 465 chain with increasing spatial resolution. The model chain, with the nest-  
 466 ing of a phase-resolving model into a phase-averaged model, provides an

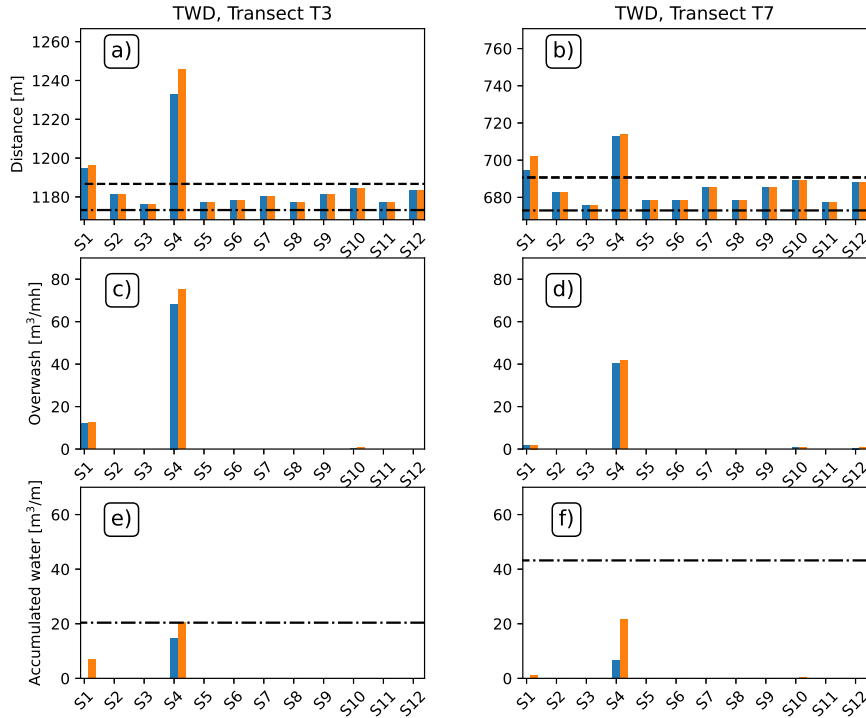


Figure 13: Comparison of the results from XBeach simulations using the permeability coefficient of 0.0003 m/s (blue) and using the permeability coefficient of 0.00003 m/s (orange). a) and b) Horizontal total water distance TWD. The dashed line is the berm crest location, whereas the dot-dashed line is the intersection between the mean water level and the beach profile. c) and d) Cumulative overwash volume. e) and f) Accumulated water volume over the emerged beach at the end of the simulation. The dot-dashed line is the maximum water volume that can be stored between the berm and the dune system.

467 accurate characterization of the main nearshore and shallow water processes  
 468 driving wave runup dynamics, limiting the number of assumptions involved.  
 469 However, few assumptions are still present in the XBeach simulation setup.  
 470 For instance, the cross-shore configuration precludes the characterization of  
 471 longshore dynamics. The validity of the cross-shore approach in surf zone  
 472 modelling has been extensively addressed by Fiedler et al. [27, 21]. In par-  
 473 ticular Fiedler et al. [27] tested the 1D assumption and concluded that it  
 474 is a reasonable assumption for the prediction the bulk properties of runup  
 475 observed on natural beaches for a wide range of incident wave conditions.  
 476 In fact, as long as the offshore boundary of the 1D model lies outside the

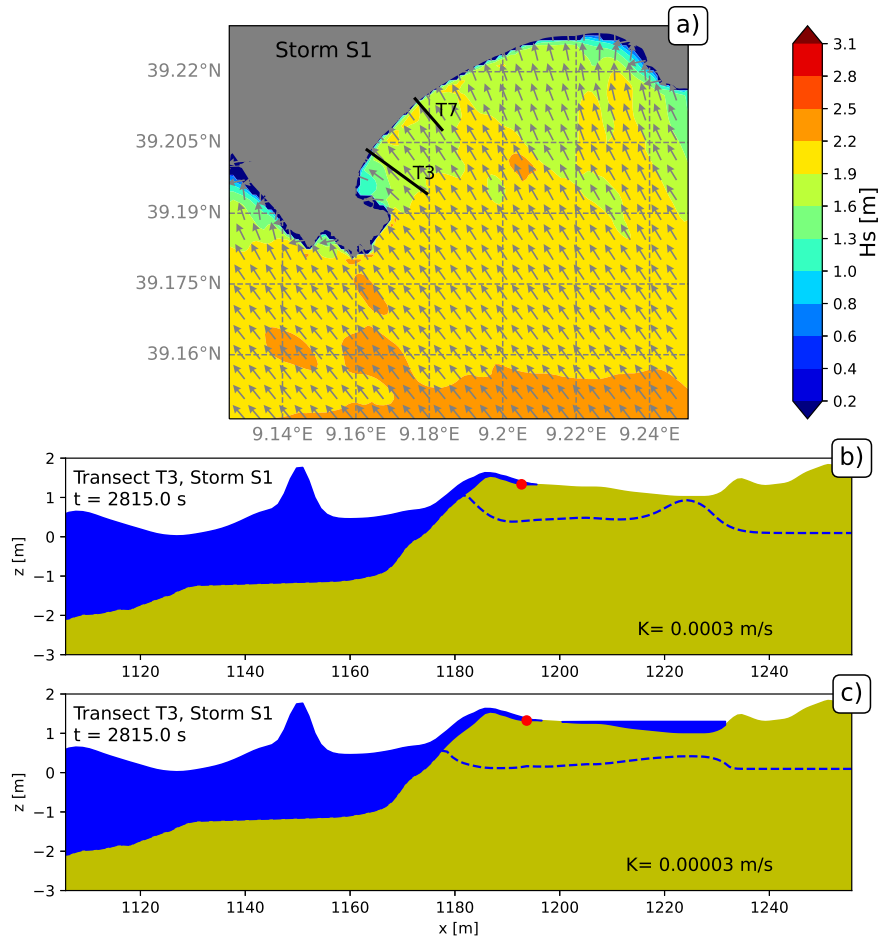


Figure 14: a) Significant wave height field computed by SWAN for storm S1. b) and c) Snapshot of the XBeach simulations for Storm S1 along the transect T3 with a permeability coefficient ( $K$ ) equal to 0.0003 m/s and 0.00003 m/s, respectively. The red dot shows the moving shoreline (runup) location. The blue dashed line indicates the groundwater table elevation.

477 surf zone but sufficiently close to the shoreline (in this study it lies at a  
 478 point with 14 m depth), refraction processes of shoaling waves lead to a near  
 479 normal wave incidence at this boundary.

480 A good agreement is found between the vertical runup values calculated  
 481 with the empirical formulation by Stockdon et al. [23] and those computed  
 482 with XBeach, see Figure 10. Among different runup formulations that have

483 been proposed during the last decades [28, 29], we have chosen to apply the  
484 Stockdon et al. [23] formulation due to its wide diffusion within the coastal  
485 engineering community [30, 31]. Although empirical formulations still lack  
486 to address the effects induced by complex nearshore morphology [32, 33] and  
487 by incoming wave features [34, 35], they have proven to provide a first order  
488 assessment of wave runup under a wide range of wave and environmental  
489 conditions [36]. This justifies their use for a first order assessment of runup  
490 in those situations in which the use a phase-resolving model is not recom-  
491 mended, for instance for operational systems whose routines are run daily  
492 and computational efficiency is of paramount importance [18].

493 Previous studies have reported highly dynamic banquettes that evolve,  
494 form and recede according to the wave forcing variability [37, 8, 38, 9]. Al-  
495 though the evolution of beach-cast *Posidonia oceanica* litter has been widely  
496 reported, fewer studies have addressed dynamics of small woody debris and  
497 reed deposits. Gómez-Pujol et al. [38] and Trogu et al. [9] showed that the  
498 permanence of banquettes on wave-exposed beaches is transitory and these  
499 features hardly withstand energetic storms. This variability raises doubts  
500 about the effective coastal protection offered by seagrass wracks under storm  
501 conditions. Nevertheless, observations of the berm dynamics during the win-  
502 ter and spring 2019-2020 at Poetto suggest that major storms are able to  
503 shift shoreward the organic berm location but not to dismantle it (see Fig-  
504 ure 15 showing the presence of reed wracks both before and at the end of  
505 storm S4). In other words, the presence of intertwined reeds and seagrasses  
506 within the beach berm seems to increase its flexibility and preserve it against  
507 destructive wave action. More detailed analyses on the variability of the ex-  
508 tension of reed and seagrass wracks according to wave and environmental  
509 forcing will be presented in a future paper.

510 Since the larger permeability coefficients have been found in areas with  
511 sand mixed with buried reeds, this result suggests that intertwined reed and  
512 seagrass wracks can mitigate the effects of overwash and flooding by increas-  
513 ing the beach permeability, promoting infiltration and thus water evacuation  
514 from the emerged beach. [In this study, the effects of a locally-increased  
515 bottom friction by reed ad seagrass deposits seems to have a limited and  
516 secondary impact on coastal flooding.](#) The discussed assumptions involved  
517 in this study, such as the use of a single permeability coefficient over the  
518 entire beach profile, suggest that these findings should be confirmed by more  
519 refined and more exhaustive swash modelling in future works.

520 [In terms of coastal protection from flooding, these results suggest that](#)



Figure 15: View of the Poetto beach from the video camera system. a) picture taken before S4 storm (19/01/2020); b) picture taken at the tail of S4 storm (24/01/2020).

521 keeping the reed deposits in place appears as a sound solution. The reed  
522 deposits can be regarded as an ecosystem-based solution and their services  
523 be should be taken into account in a sustainable coastal planning strategy.  
524 At the same time, it is evident that these barriers of dead plants on Mediter-  
525 ranean beaches considerably limit the suitability for bathing. Therefore, in

526 these cases, their removal must be considered, creating the problem of rec-  
527 onciling environmental protection and tourist use. In this context, making  
528 available to local authorities an assessment of how the reed and seagrass  
529 deposition affects coastal processes can be beneficial towards a sustainable  
530 coastal management. In principle, the the same approach adopted by the  
531 legislation for the *Posidonia oceanica* management can be extended to reed  
532 wracks: keeping the biomass in place, compatibly with the touristic voca-  
533 tion of a specified beach. In fact, the intertwined reed and seagrass wracks  
534 have the effect of increasing the permeability of the beach, thus favouring  
535 the drainage of water from the emerged beach, eventually reducing flood-  
536 ing. Nevertheless, in this particular case, the touristic vocation of Poetto  
537 beach precluded the possibility of keeping the huge amount of reed deposits  
538 in place, as they constituted a significant obstacle in terms of beach fruition  
539 and shoreline accessibility.

## 540 **7. Conclusions**

541 This work devotes a special attention to runup processes induced by  
542 storms at a low-lying backbeach in the presence of reed and seagrass de-  
543 posits. The methodology included a model chain with increasing spatial  
544 resolution and details. Data showed that, due to the beach profile with the  
545 berm higher than the emerged beach, the horizontal runup provided a quan-  
546 tification of the flooding extension that is more difficult to achieve from the  
547 vertical runup. Using the hydraulic conductivity parameter measured in a  
548 beach area with sand and buried reeds, infiltration processes allowed the  
549 beach to drain the overwashed water and its return to the sea. The role  
550 of beach permeability on runup was assessed by running a new set of wave  
551 simulations using a low hydraulic conductivity parameter, equal to that mea-  
552 sured in a beach area with sand only. Under overwash conditions, runup and  
553 flooding extensions were increased by a low permeability coefficient. These  
554 results highlight the role of the ecosystem services provided by intertwined  
555 reed and seagrass wracks on beaches, suggesting that they must be taken  
556 into account in a sustainable coastal planning strategy.

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