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1 A cascade biorefinery for grape marc: recovery of materials and energy through

2 thermochemical and biochemical processes

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- 14
- 15 Abstract:

16 The agro-industrial sector makes a high contribution to greenhouse gas emissions; therefore, proper waste 17 management is crucial to reduce the carbon footprint of the food chain. Hydrothermal carbonization (HTC) is 18 a promising and flexible thermochemical process for converting organic materials into energy and added-value 19 products that can be used in different applications. In this work, grape marc residues before and after an 20 extraction process for recovering polyphenols were hydrothermally treated at 220 °C for 1 h. The resulting 21 hydrochar and process water were investigated to test an innovative cascade approach aimed at a multiple 22 product and energy recovery based on the integration of HTC with anaerobic digestion. The results show that 23 this biorefinery approach applied to grape marc could allow to diversify and integrate its potential valorisation 24 options. The produced hydrochars possess an increased fixed carbon content compared to the feedstock (up 25 to +70%) and, therefore, can be used in soil, immobilizing carbon in a stable form and partially replacing peat 26 in growing media (up to 5% in case of hydrochar from grape marc after extraction), saving the consumption of 27 this natural substrate. In addition, energy can be recovered from both hydrochar by combustion and from 28 process water through anaerobic digestion to produce biogas. Hydrochars show good properties as solid fuel

similar to lignite, with an energy content of around 27 MJ kg⁻¹ (+30% compared to the feedstock). The anaerobic digestion of the process water allowed obtaining up to 137 mL of biomethane per gram of fed COD. Finally, while HTC process waters are suitable for biological treatment, attention must be paid to the presence of inhibiting compounds that induce acute toxic effects in aerobic conditions. The proposed approach is consistent with the principles of circular economy and could increase the overall sustainability and resilience of the agro-industrial sector.

35

36 Keywords: Hydrothermal Carbonization, Biofuel, Soil Amendment, Biomethane, Biorefinery.

37

38 1. Introduction

39 The food supply chain is one of the foundations of human society. Its intrinsically positive role, however, is 40 jeopardized by economic, environmental, and social issues, such as: vulnerability to natural calamities; uneven 41 availability of food and fertile land; overuse of land and water resources and related morphological and 42 hydrographic impacts; threats to ecosystems and loss of biodiversity; overuse of pesticides to increase 43 productivity. Over the last few decades, the food supply chain exacerbated the climate emergency. Globally, 44 the food sector account for more than one-third of total global anthropogenic greenhouse gas emissions (3-7 45 of the 11-19 billion tons of emissions per year) as estimated by the Intergovernmental Panel on Climate change 46 (Crippa et al., 2021). Although land use and production, including fertilizers use, are still the main contributor 47 to agricultural emissions, packaging, transport, "cold chain" activities, processing, and related energy 48 consumption and waste production all play an increasingly large role (Crippa et al., 2021). Reducing the food 49 chain carbon footprint is central to addressing climate change, and proper waste management is of particular 50 importance (Karl & Tubiello, 2021). Improper waste management is pushing the food supply chain to the top 51 of the list of greenhouse gas emitters, as reported by the United Nations Agriculture Agency during the COP26 52 climate conference in Glasgow in 2021. However, the organic nature of most of the residues produced along 53 the food supply chain is suitable for innovative valorization processes consistent with the principles of the 54 circular bioeconomy.

It is important to develop processes and approaches to flexibly recover both material and energy resources, in accordance with the needs of local and regional market (Muntoni, 2019). In the case of agro-industrial waste, it is ideal if the recovery of resources addresses concomitant problems, such as the need for renewable energy sources to alleviate increasing energy demands of the food chain, and renewal soil amendments to preserve

and restore the carbon balance of the soil (Fryda et al., 2018).

60 Worldwide, 260 million hectolitres of wine were produced in 2020, which is in line with the yearly average 61 production over the last decade. For every 100 kg of grapes, about 70 litres of wine and 18 kg of grape marc 62 are produced. Accordingly, over 6 million tons of grape marc are produced globally every year (OIV -63 International Organisation of Vine and Wine Intergovernmental Organisation, 2021).

64 The management of such a large amount of biowaste, enriched in water (around 60% by weight) and 65 organic matter (up to 900 g kgTS⁻¹) and characterized by an acidic pH (3-6), and high lignin and polyphenol 66 content is a task that must be faced consistently, made more challenging by the constraints of current 67 environmental and economic policies. Furthermore, management options must consider the seasonality of 68 production since approximately 75% of solid waste is generated during the harvest period (around 2 months). 69 Grape marc is sometimes used as a by-product, e.g., for ruminant animal feeding, although some adverse 70 effects may occur due to the presence of substances such as polyphenols (Baumgärtel et al., 2007; Devesa-71 Rey et al., 2011; Pinelo et al., 2006). Grape marc can be managed using biological treatments such as 72 anaerobic digestion, with reported methane yields spanning 113 - 420 L CH₄ kgVS⁻¹, or via composting and 73 subsequent use on soil. The relatively high heating value of grape marc (19 - 22 MJ kg⁻¹) would support its use 74 in direct combustion scenarios (Muhlack et al., 2018); however, the high water content makes pre-drying 75 necessary.

76 This study proposes an integrated approach for the sustainable management of grape marc and evaluates 77 valorization options that combine the recovery of materials and energy by coupling different processes such 78 as hydrothermal carbonization and anaerobic digestion, investigating multiple by-products valorization 79 pathways. Hydrothermal carbonization (HTC) is a wet thermochemical process that rapidly converts organic 80 substrates into added-value by-products. Under autogenous pressures and temperatures generally ranging 81 from 180 to 250 °C, a coal-like solid material known as hydrochar and process water are produced, whose 82 characteristics suggest a wide range of potential applications (Libra et al., 2011). During the process, water 83 acts as both the reaction medium and catalyst, making HTC suitable for wet biomass valorization.

Hydrothermal carbonization technology is sustainable as it embraces the principles of a circular economy and is a waste management system capable of lowering climate-altering emissions. In its most typical application, biomass-derived hydrochar is used as a fuel for renewable energy production, acting as a neutral combustible and energy-dense carbon source. Being a carbon-enriched solid, hydrochar combustion involves lower CO₂ emissions per unit of energy developed compared to the combustion of the raw material, further offsetting CO₂ emissions. The chemical-physical characteristics of hydrochar make its application interesting also as a soil amendment, able to improve fertility as well as water retention and carbon sink (Funke & Ziegler,
2010; Libra et al., 2011; Wang et al., 2018).

Besides the hydrochar, the process water may be the bottleneck in view of an industrial up-scaling, since it is still understudied in terms of its sustainable management (Ipiales et al., 2021). Due to the high organic load of process water, it may be a suitable substrate for anaerobic digestion to produce biomethane. Recently, several studies proposed the integration of hydrothermal carbonization with anaerobic digestion as a flexible and circular system to exploit the recovery potential of waste materials (Catenacci et al., 2022; Ipiales et al., 2021).

98 Few studies are reported in literature focusing on grape marc treated via HTC. Basso et al. (2016) treated 99 grape marc (solid-liquid ratio of 1:10) at 180, 220, and 250 °C for 1, 3, and 8 h in a small-scale reactor (50 mL) 100 reporting increasing carbon content and reduced ash and oxygen content in hydrochar (HC). At the same 101 conditions (Baratieri et al., 2015) developed a thermal dynamic model based on the solid yield obtained after 102 HTC of grape seeds. Same results were stated by Nguyen et al. (2022) and Mäkelä et al. (2017) who worked 103 at similar temperatures (180, 220, and 260 °C) for 0.5 h in a 0.5 L pressurized reactor using an initial solid 104 content of 40 and 25 wt%, respectively. Basso et al. (2018) investigated the behavior of grape marc 105 components (seeds and skins) treated at 180, 220, and 250 °C for 0.5, 1, 3, and 8 h using a 50 mL reactor. 106 Mariuzza et al. (2022) applied HTC to different residues, including grape marc, at 220 °C for 1 h in a 50 mL 107 reactor using a solid liquid ratio of 1:5. Other thermochemical processes have also been applied to grape marc: 108 Lin et al. (2021) studied the valorization of this residue and its mixture with other materials (such as cow manure 109 and HCs) via pyrolysis.

The available studies, all conducted in small-volume reactors (< 0.5 L), demonstrate the possibility of using the hydrochar from grape marc in different applications; however, no information is yet available on the management of the produced process water and, to the best of our knowledge, on the potential integration of HTC and anaerobic digestion for the valorization of this residue.

The specific objective of this work is to assess i) the potential application of the hydrochar produced via HTC from grape marc as a soil improver and solid fuel, and ii) the biological treatability (anaerobic and aerobic) of the process water in view of energetic valorization or disposal. Hydrothermal carbonization was performed on both raw grape marc (GM) and GM after extraction of polyphenols (GM_Ext), compounds that find application in different production sectors.

To achieve the study's objective, cascade processes and treatments were applied; HTC tests were carried
 out at a temperature of 220 °C for 1 h. After HTC, the products were tested through different valorization

pathways. The feasibility of hydrochar as a solid fuel and as soil improver or peat substitute was investigated,
while assessing the suitability of process water as substrate for energy recovery via AD, or for its treatment in
a traditional wastewater plant.

- 124
- 125 2. Materials and methods

126 2.1 Feedstock

127 Grape marc (GM) considered in the study consists of skins, stems, and seeds from winemaking with the 128 Cannonau cultivar collected in southern Sardinia (Italy). The GM was dried at 40 °C for about 48 h and stored 129 in the dark at 4 °C in vacuum plastic bags. Considering the significant presence of bioactive molecules in GM, 130 especially polyphenols, their extraction and recovery may be functional to manufacturing nutraceutical and 131 pharmaceutical products for human health (Manca et al., 2020). To this aim, polyphenols separation was 132 carried out through preliminary particle size reduction followed by solid-liquid extraction using a hydroethanolic 133 mixture in a previous study (Perra et al., 2021). Briefly, a part of the dried GM was grinded to obtain a powder 134 with a diameter between 16 and 515 µm, measured with a laser diffraction particle size analyser (Mastersizer 135 3000, Malvern Panalytical Ltd, Worcestershire, UK), using the wet dispersion method and distilled water as 136 dispersant. 100 g of GM was suspended in 1 L of a mixture of ethanol and water (70:30 v/v, density 0.885 g 137 mL-1), and left under stirring conditions in the dark at 25 °C for 48 h. The dispersion was centrifuged two times 138 (30 min, 8000 rpm) to separate solid and liquid fractions. The exhausted GM (GM Ext) was recovered as 139 feedstock material for the HTC process.

140

141 2.2 Hydrothermal carbonization

142 Hydrothermal carbonization was carried out in a 1.5 L stainless steel pressurized reactor (Berghof, BR-1000). 143 The reactor was equipped with an electric jacket for heating, a thermocouple for the continuous monitoring of 144 the inside temperature, a stirred shaft and a data logging unit connected to a computer where the main 145 operating parameters (inner temperature and autogenic pressure) were continuously recorded. GM and 146 GM Ext were both treated at 220 °C for 1 h (with a temperature increase of 2 °C min⁻¹). These conditions were 147 selected to balance the conversion performance and the energy consumption. Cellulose and lignin hydrolysis 148 is significant at above 200 °C (Funke & Ziegler, 2010; Libra et al., 2011) and 1 h treatment may assure a proper 149 conversion (high solid yield (Libra et al., 2011) with minimal energy usage. These hypothesis are also confirmed 150 by Lucian & Fiori, (2017) who defined 220 °C for 1 h as the most favourable conditions. The solid material with 151 its moisture content (6.17 ±0.68 wt% and 7.40 ±0.57 wt% for GM and GM Ext, respectively) was placed in the 152 reactor together with distilled water to achieve a solid content of 10 wt% (1 kg of total input mass) filling the 153 reactor at ca. 75% of its volume. After the input material preparation, the reactor was sealed, and the controller 154 was set to the desired temperature and holding time. Once reactor was kept at 220 °C for 1 h, it was turned off 155 and cooled to room temperature overnight (the temperature profile during the cooling phase is reported in 156 Figure S1 in Supplementary Material). Before unsealing it, the final inner pressure was noted and the gas 157 released evaluated through a column gas meter, based on water displacement method, to estimate the volume 158 produced. To assure a mass balance as precise as possible, all the output materials were carefully weighed 159 before and after each step. The carbonized sludge resulting from the HTC process was separated through a 160 press filter obtaining the solid (hydrochar, HC) and the liquid (process water, PW) phases. The hydrochar was 161 stored in vacuum plastic bags at 4 °C while the process water was vacuum filtered at 0.45 µm and stored in 162 plastic bottles at 4 °C. All tests were carried out three times to ensure replicability. According to the feedstocks, 163 the hydrochars were named HC GM and HC GM Ext and the process water samples PW GM and 164 PW_GM_Ext.

The hydrochars produced were characterized in terms of moisture content, ash content, elemental composition, density, surface chemistry and higher heating value (HHV). The moisture in hydrochar after separation from the liquid phase was estimated by heating three samples (randomly selected from the total mass) to 105 °C. The volatile matter, ash content, and fixed carbon were measured through thermogravimetrical analysis (TGA – 710, LECO). Further analyses (i.e., CHN/S, HHV, and FT-IR) were conducted on representative dried and milled samples as detailed in the Supplementary Material. Oxygen was evaluated by difference from C, H, N, S, and ash.

The liquid phase from the HTC runs was characterized in terms of pH and electrical conductivity (EC), total organic carbon (TOC), and chemical oxygen demand (COD). Details on methods are available in Supplementary Material. All the measurements for both solids and liquids were performed 3 times at least and the results were validated through statistical pairwise t tests (significance level α = 0.05) performed using the software JMP (v. 15, SAS).

177

178 2.3 Germination test

According to the standard test UNI EN 16086-2:2012-01, Sphagnum peat, previously sieved at 10 mm, was mixed with dried GM, HC_GM, and HC_GM_Ext. 5, 25, and 50 wtdb% of feedstock or hydrochars were mixed with peat. The samples were named with the codes formed by the initials of the material mixed with the peat and the used amount; to give an example, the sample with the mixture containing peat and 5% hydrochar from 183 grape marc was labelled HC GM 5%. Moisture was checked and adjusted with the fist test, adding water until 184 squeezing the material with the fist did not produce leaching. Around 50 g of each mixture were placed in 3 185 square Petri dishes and 10 seeds of cress (Lepidium sativum L.) were sown at the top of the dish. In addition, 186 3 more Petri dishes filled with only peat were used as a control. One drop of water was added to each seed. 187 Petri dishes were closed with parafilm and stored in an oven at 25 °C for 72 h for incubation with an inclination 188 of 70 – 80° (seeds at the top). After 72 h of incubation, the Petri dishes were opened, the germinated seeds 189 were counted, and the length of the seedlings was measured. The germination rate was defined as the 190 percentage of germinated seeds on the total number of seeds. The results were validated with statistical tests, 191 such as ANOVA and Tukey's HSD test through the statistical software JMP (v. 15, SAS). Several parameters 192 were calculated: average germination rate (AGR), coefficient of variance for germination rate (CVG), average 193 root length per plant (ARLP), coefficient of variance for root length (CVR), average hypocotyl length per plant 194 (AHLP), coefficient of variance for hypocotyl length (CVH), root length index (RI), and Munoo-Liisa vitality index 195 (MLV).

196

197 2.4 Assessment of material stability

Several methods have been proposed to measure biomaterial stability. Among them, respirometric methods based on oxygen consumption are broadly recommended (Sánchez Arias et al., 2012). Electrolytic respirometry is based on the Warburg manometric respirometer and is usually referred to as the Sapromat[®] system. This system has been extensively applied to estimate O₂ consumption for various purposes/fields: biodegradability of waste and wastewater, toxicity, and inhibition tests, modelling and kinetics of biodegradation, respiration of polluted soils, compost and biologically pretreated waste stability.

204 10 g of pre-humidified HC were placed in a 500 mL glass reaction bottle, connected to an oxygen generator 205 and a pressure control gauge. The bottle rests in a water bath (20 °C). During aerobic degradation, 206 microorganisms consume oxygen and produce an equivalent amount of carbon dioxide. CO₂ is continuously 207 adsorbed by around 5 g NaOH granules, placed in a small container integrated in the reactor bottle, resulting 208 in the establishment of a negative pressure in the bottle. Oxygen is electrolytically produced until the negative 209 pressure is compensated. The amount of produced oxygen is calculated by the required electric energy 210 (according to Faraday's Law), which is recorded in intervals of 36 s by the control unit (Binner et al., 2012)... 211 The tests were run in triplicate.

The HC stability was assessed in relation to RA₄ (total oxygen consumption after 4 days), which is the recommended parameter for the estimation of compost stability by the European Union (European

214 Commission, 2001).

215

216 2.5 Assessment of Biochemical Methane Potential (BMP)

217 The BMP measurement is a standard test for determining biogas production from an organic substrate using 218 methanogenic bacteria as the inoculum under optimal batch conditions. This test was applied to the PW 219 produced during HTC for assessing the possibility of conversion into biogas, according to the standard 220 UNI1601755EIT, BMP tests were conducted in brown glass bottles, where methanogenic sludge was mixed 221 with HTC PW. The methanogenic inoculum for biochemical methane potential (BMP) tests was collected from 222 a mesophilic anaerobic digestion plant treating cattle slurry and grass silage located in southern Sardinia (Italy). 223 The amount of sludge and sample was set to allow gas to form in the headspace of the bottles and ensure a 224 food-microorganism ratio (F/M) of 0.5 gCOD gCOD⁻¹ according to the literature (Boulanger et al., 2012; Pagés-225 Díaz et al., 2020). Methanogenic sludge with D-glucose was used to assess the specific methanogenic activity 226 (SMA, data not shown). A blank was used with only inoculum. No nutrient solution or pH buffer was added to 227 the bottles. The initial pH value was around 7.0 for all samples. All the tests were performed in triplicate. Before 228 the bottles were sealed with airtight caps, they were purged with nitrogen to ensure anaerobic conditions. The 229 sealed bottles were placed in a thermostated shaker (T = 39 ± 1 °C) and kept for 36 days. An average period 230 of 3 days was adopted, slightly shorter at the beginning of the test and longer at the end, to purge the gas 231 produced and accumulated in the reactors. Partial and cumulative biogas production was measured over time. 232 The volume produced was measured through a water-displacement method using a volumetric column, and 233 the gas samples were analyzed using a GC-FID (7890B, Agilent Technologies) equipped with a thermal 234 conductivity detector (TCD) and two stainless columns packed with HayeSep N (80/100 mesh) and Shincarbon 235 ST (50/80 mesh) connected in series.

236 The methane yield at 36 days was calculated as follows (Eq. (1)):

237

$$BMP = (V_{CH_4,s} - V_{CH_4,blank})/COD_s$$
(1)

238

 $V_{CH4,s}$ is the volume of methane produced from the PW measured at the end of the test, $V_{CH4,blank}$ is the volume of methane produced from the inoculum measured at the end of the test and COD_s is the mass of soluble COD contained in the volume of added PW. The modified Gompertz equation, based on a sigmoid function, was used to predict the methane production and calculate the kinetic parameters, according to Eq. (2) (Pagés-Díaz et al., 2020). This model was originally developed to describe the slowdown of the batch reactor culture of any microorganism and was modified by Zwietering et al. (1990) by incorporating the classic parameters of maximum concentration, latency time and maximum growth rate. The modified Gompertz model assumes that the methane production is proportional to microbial activity (Nielfa et al., 2015).

$$Y(t)CH_4 = Y_{max}CH_4 exp\left\{-exp\left[\frac{R_{max} \cdot e}{Y_{max}CH_4}(\lambda - t) + 1\right]\right\}$$
(2)

248

Y(t)CH₄ is the cumulative production yield of CH₄ at time t, Y_{max}CH₄ is the maximum theoretical production yield, R_{max} is the maximum production rate, λ is the duration of the lag phase, t is the time and 'e' is the Neperian number. The experimental data were fitted through Eq. (2) using the TableCurve 2D[®] software (v. 5.01, Systat Software Inc.) through least-squares non-linear regression. The coefficient of determination R² was used to preliminary evaluate fitting accuracy of Gompertz model for each experimental dataset.

254

255 2.6 Assessment of acute toxicity

256 A pH-stat titration unit (ANITA, Ammonium NITrification Analyser) was used to assess the acute inhibiting 257 effect of HTC process water on the ammonium-oxidizing bacterial community in activated sludge, as described 258 in Ficara & Rozzi (2001). The tests were carried out in a glass vessel containing 1 L of unacclimated activated 259 sludge (total suspended solids, TSS, 4 g L⁻¹) drawn from the Oristano wastewater treatment plant (Italy). The 260 maximum ammonium-oxidizing capacity of nitrifying biomass was measured in the presence of ammonium as 261 the only substrate, considering the stoichiometric relationship between ammonium oxidation and acidity 262 production, and used as reference. Known volumes of PW GM and PW GM Ext were added to the activated 263 sludge every 20 minutes. The resulting nitrifying activity was compared with the reference and the 264 corresponding inhibition was calculated for each dosage. At the end of the test, nitrification was fully inhibited 265 by allylthiourea to detect the presence of interferences. A dose-response curve was plotted for both PW GM 266 and PW_GM_Ext according to Eq. (3), and the IC₅₀ (that is the amount of PW that causes 50% acute inhibition 267 of sludge activity) was determined.

$$I(\%) = \left(1 - \frac{1}{1 + \frac{d^a}{b}}\right) 100$$
(3)

I is the inhibition expressed as percentage, d is the dose in mL L⁻¹ and a and b are curve parameters
which are obtained by fitting the experimental data.

271

272 3. Results and discussion

273 3.1 Characterization of feedstock and products

The main properties of the two materials used as feedstock for the HTC runs and the characterization of the hydrochars are shown in Table 1. All parameters were evaluated on a dry basis by weight, apart from the moisture content.

277 After the HTC tests, a solid yield (Y) of 62.28 wtdb% (±0.69) was found for GM Ext, while a slightly lower 278 value of 59.59 wtdb% (±0.52) was obtained in the tests on GM. This is consistent with the extraction process 279 previously applied to GM Ext, which may have involved the removal of soluble compounds from the solid 280 matrix. Literature reports solid yield ranging from around 50 and 75 wtdb% under different operating conditions 281 (Basso et al., 2016; Mäkelä et al., 2017). Mariuzza et al. (2022) obtained a solid yield of 69.2 wtdb% (±1.3) at 282 the same temperature and duration used in our experiments. However, it must be highlighted that the 283 experimental conditions differed for the size reactor (30 times smaller than ours) and for the cooling phase, 284 that was quicker compared to the one applied in our study. The cooling conditions could affect the final yield 285 and properties of the produced materials due to the formation of a secondary char on the surface of the primary 286 char as suggested by different authors (Benavente et al., 2022; Lucian et al., 2018). However, due to the 287 reactor characteristics, we studied the HTC process considering the material deriving from the natural cooling 288 phase without accelerating it. While considering the given limitations related to the cooling phase, our solid 289 yields are placed within the range reported in literature.

In comparison to the feedstock, the ash content and the volatile matter in the produced HCs was lower and fixed carbon higher, aspect of interest in view of the use of HC as a fuel and as a carbon replenishment in soil. Regarding the elemental composition, carbon relative content increased, while nitrogen and oxygen ones decreased under the carbonization process. No significant differences were found between the feedstocks (p > 0.05), apart for volatile matter (p = 0.023) and fixed carbon (p = 0.012). All parameters analysed in HC reported significant differences compared to the feedstocks (p < 0.001), except for hydrogen (p > 0.05).

Hydrochars reported significant differences in the solid yield only (p < 0.001).

Material	Code	Solid	Moisture	Volatile	Ash	Fixed	С	Н	N	0	
		yield [%]	[wt%]	matter [wt%]	[wt%]	carbon [wt%]	[wt%]	[wt%]	[wt%]	[wt%]	kg
Grape marc	GM		6.17	71.19	7.64	21.17	49.00	6.09	2.08	35.19	
			(0.07)	(0.08)	(0.18)	(0.10)	(0.15)	(0.08)	(0.13)	(0.13)	(
Grape marc	GM_Ext		7.40	73.24	8.13	18.64	49.63	5.94	2.09	34.22	
(extracted)			(0.56)	(0.17)	(0.46)	(0.29)	(0.29)	(0.08)	(0.13)	(0.23)	(
Hydrochar	HC_GM	59.59		63.53	3.96	32.51	61.60	6.14	1.85	26.45	2
from GM		(0.52)		(0.48)	(0.04)	(0.52)	(0.60)	(0.15)	(0.11)	(0.76)	(
Hydrochar	HC_GM_Ext	62.28		64.95	3.33	31.72	62.46	6.28	1.68	26.25	2
from GM_Ext		(0.69)		(1.02)	(0.01)	(1.00)	(0.29)	(0.12)	(0.07)	(0.32)	(

Table 1. Main properties of grape marc, extracted grape marc, and hydrochars. STD is reported in brackets.

298

Results are reported on dry basis; moisture on wet basis.

To assess potential modifications induced by HTC on the chemical functions of the materials, ATR-FTIR spectra were recorded on samples before and after the hydrothermal treatment. Figure S2 reports a comparison between the spectra of the GM powder and of selected seeds, stems, and skin, for starting material characterization.

303 The spectrum of GM consists of the typical peaks reported for polyphenolic lignocellulosic and flavonoid 304 compounds found in grape marc (Casazza et al., 2016), together with a contribution of amines as the result of 305 biogenic decarboxylation processes of amino acids (Grossmann et al., 2007). Details on the peaks attribution 306 are reported on the spectra (Figure S2). In summary, the typical peaks related to lignin and polyphenols - OH 307 (υOH 3300s-br when secondary H-bonding are present, δOH 1378m, υPhO 1263s), C-H (aliphatic CH: υ 2980-308 2850mw, δ/ρ 1400-1300m; aromatic CH: δ 650-720m), C=C (aliphatic C=C: υ 1650m; aromatic C=C: υ 1540m) 309 and C-O (vC=O 1750m; vC-O 1026s; vC-O-C 1130m), as well as those typical for amines (vNH 3313m and 310 3271m; \deltaNH 1600m-br; vCN 1063s), are present (Fan et al., 2012). A comparison of the GM and GM Ext IR 311 spectra is reported in Figure 1a, showing no significant modification in the spectrum profile after solvent 312 extraction. A significant modification of the chemical composition and structure of both feedstock seems 313 occurring during the HTC process as highlighted by the comparison of the spectra reported in Figure 1b, for 314 GM and HC_GM, and Figure S3 for GM_Ext and HC_GM. In agreement with the loss of oxygen and nitrogen

found in the samples after HTC, the peaks related to the phenolic moieties of polyphenols and their intermolecular secondary interactions, as well as those of possible carboxylic groups and NH₂ stretching vibrations (vNH 3271 and 3313 cm⁻¹) are mainly reduced. Correspondingly, peaks typically related to unsaturated aromatic and aliphatic C=C bonds (1650-1598 cm⁻¹) and aromatic CH in bonds (719 cm⁻¹) increased.

The main characteristics of the process water are reported in Table 2. The HTC treatment led to an acidic pH and an electrical conductivity (EC) value of around 12 mS cm⁻¹ for both the PW, typical features of the liquid phase from HTC (Funke & Ziegler, 2010; Libra et al., 2011). The total organic carbon (TOC) accounted for 9.69 g L⁻¹ for PW_GM and 7.68 g L⁻¹ for PW_GM_Ext. Similarly, the soluble COD was higher in GM than GM_Ext, with values higher than 30 gO₂ L⁻¹. The combined analysis of the characteristics of HC and process water suggests that the preliminary extraction treatment slightly enhances the fixation of carbon in the HC, limiting its release into the PW.

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- 329



pH [-] TSS [g L⁻¹] COD [gO₂ L⁻¹] Sample EC [mS cm⁻¹] NVSS [g L⁻¹] TOC [g L⁻¹] 33.28 (0.42) PW GM 4.40 (0.02) 12.52 (0.88) 24.73 (0.01) 9.69 (0.33) 9.84 (0.99) 31.08 (0.97) PW GM Ext 4.37 (0.08) 11.37 (0.16) 21.59 (0.02) 8.90 (0.36) 7.68 (0.48)

332 Table 2. Process water characterization (average of triplicates). STD is reported in brackets.

EC = electrical conductivity; TSS = total suspended solids; NVSS = non-volatile suspended solids; TOC = total organic
 carbon; COD = chemical oxygen demand.

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336 The product mass distribution in the solid, liquid and gas phases observed after the HTC treatment is 337 reported in Table 3. The response to the conditions of the HTC process was similar for the two types of grape 338 marc, regardless of the preliminary extraction. As described in 2.2, the solid content at the beginning of the 339 HTC test was 10%. The treatment resulted in a dramatic reduction of the solid phase with a modest gasification. 340 The solid reduction was likely due to both to dehydration reactions and solid mass solubilisation, the latter 341 resulting in an increased density of the liquid solution. As for the fate of the inorganics, as much as 69.11 and 342 74.49 wtdb% of the initial ash content of the GM and GM Ext, respectively, was solubilised in the process 343 water.

344 Table 3 Solid, liquid and gas mass fractions after HTC treatment. STD is reported in brackets.

		
Phase	GM [wt%]	GM Ext wt%
Solid (Hydrochar)	6.05 (0.07)	6.32(0.08)
		0.02 (0.00)
Liquid (Brooses water)	02.05 (0.12)	02 79 (0 05)
Liquid (Frocess water)	92.05 (0.13)	92.76 (0.05)
Gas	1.10 (0.06)	0.90 (0.03)
	()	()

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The results of the characterization analyses of the phases that result from the HTC treatment were used to perform mass balances for the elements carbon and nitrogen according to equation 4.

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$$M_{\rm IN} = M_{\rm HC\,OUT} + M_{\rm PW\,OUT} + M_{\rm GAS\,OUT} = M_{\rm OUT}$$
(4)

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350 The carbon and nitrogen distributions in the HTC products are presented in Figure 2, where the gas phase 351 was evaluated considering the measured volume and the density of CO_2 (1.87 kg m⁻³). Most of the carbon is present in the solid phase, to a higher extent in the sample derived from GM_Ext while the carbon dissolved in the liquid phase is higher for the samples derived from GM. In contrast, nitrogen is almost uniformly distributed among the solid and liquid phases, as far as the latter is counted as a complement to 100 and assuming zero nitrogen in the gaseous phase, since the HTC gas is mainly composed by CO_2 (> 95%), CO, and H₂ (Libra et al., 2011).

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363 3.2 Potential valorization of hydrochars

364 3.2.1 Assessment of the energetic valorization of hydrochars

In Figure 3, a Van Krevelen diagram, The feedstocks GM and GM_Ext fall within the typical area of
biomass, while the obtained HC, as expected, approach the lignite region as a consequence of the higher
grade of carbonization. Similar results were reported by Mariuzza et al. (2022) with O/C values around
0.3 and H/C approximately 1.1.

The Van Krevelen diagram highlights the transformation induced by the process, underlying that the carbonization decreased both the atomic ratios H/C and O/C as a results of dehydration and decarboxylation reactions (Funke & Ziegler, 2010; Libra et al., 2011). This is also supported by the FTIR analyses, which show a reduction in the number of carboxylic and hydroxyl groups due to HTC. The diagram is usually used to define the quality of a solid fuel paired with the assessment of the higher heating value (HHV) data. The HHV of the samples is shown in Figure 4 along with the HHV of some common solid fuels. Through HTC, the energy content of the hydrochar (around 27 MJ kg⁻¹) was increased compared to the feedstock (around 19 MJ kg⁻¹), exceeding the values associated with the solid fuels considered. Similar HHVs were found by other authors like Mäkelä et al. (2017) and Mariuzza et al. (2022) who reported values of 26.5 and 26.26 MJ kg⁻¹, respectively.

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385 Fig. 4. HHV of feedstocks, hydrochar and some solid fuels of common use

387 3.2.2 Assessment of the potential use of hydrochar as a soil amendment

The results of the germination tests are shown in Table 4. When GM and HC GM results are compared 388 389 on the basis of the RI and Munoo-Liisa vitality index (which takes into account both the germination and 390 growth aspects normalized by the control), hydrothermal carbonization is able to produce a better 391 substrate for the germination and growth of seedlings. Replacing peat with an equivalent quantity of HC 392 slightly lowers the germination rate, yet leads to longer seedlings compared to the use of raw GM. the 393 best results were achieved for HC GM Ext. On the other hand, the higher the concentration of hydrochar, 394 the lower the germination rate, with a high inhibition effect in the samples with 50% peat substitution. 395 However, the presence of hydrochar in a percentage below 25% does not affect the germination 396 significantly, but only the growth of the seedlings. the HC_GM_Ext_5% sample achieved a high RI and 397 MLV values. In contrast, all the other samples have shown inhibition of germination and growth resulting 398 in a lower MLV (less than 80%, which is considered the inhibition threshold as reported in Maunuksela et 399 al. (2012). The lack of inhibition associated with HC GM Ext might be due to the preliminary ethanol 400 extraction of GM (Wang et al., 2022). the production of aromatic compounds during the HTC process, as 401 evidenced by the FTIR analysis, does not appear to affect the growth of the seedlings. The statistical 402 analysis derived from one-way ANOVA and Tukey's HSD test is shown in Figure 5 where each letter links 403 samples that are found to be statistically similar (p < 0.05). The statistical test confirmed that the samples 404 HC GM Ext 5% belong to the same group as the control. It may suggest that the substitution of peat 405 with a 5% hydrochar produced by HTC of extracted grape marc does not affect the seed germination and 406 seedling growth. When hydrochar concentration higher than 5% was added, a detrimental effect on 407 germination was evidenced, indicating that the use in growing medium can be carried out only to a limited 408 extent. However, in a previous study (Farru et al., 2022) we found that some post-treatment can be 409 applied to enhance the germination performance even at higher hydrochar concentrations. Also, it is 410 demonstrated by different authors (Fryda et al., 2018; Lanza et al., 2016, 2018) that the addition of char 411 to soil may replenish and store carbon in soil.

412 Table 4. Main parameters calculated in germination tests for each sample.

Sample AGR [%] CVG [%] ARLP [cm] CVR [%] AHLP [cm] CVH [%] RI [%] MLV [%]

Control	100	0	3.30	12.58	1.67	4.54	-	-
HC_GM_5%	96.66	5.77	2.19	15.92	1.74	5.47	66.26	63.67
HC_GM_25%	93.33	11.55	0.42	35.46	0.47	40.69	12.82	12.31
HC_GM_50%	0	0	0	0	0	0	0	0
HC_GM_Ext_5%	96.66	5.77	3.22	6.56	2.13	2.58	97.35	94.35
HC_GM_Ext_25%	96.66	5.77	0.89	49.78	0.70	36.30	27.20	26.74
HC_GM_Ext_50%	63.33	15.28	0	0	0.01	2.44	0	0
GM_5%	100	0	0.97	28.22	1.54	13.25	29.47	29.47
GM_25%	46.66	40.41	0.18	59.16	0.17	54.27	5.30	2.12
GM_50%	90	10.00	0	0	0.01	0.00	0	0

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416 Fig. 5 Root and hypocotyl length of seedlings in germination tests and statistical results derived by Tukey's HSD417 test.

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The HC produced from the GM is characterized by a lower respirometric activity, as evidenced by the respirometric index value RA₄, calculated between the end of the lag phase and the end of the test, of 9.95 mgO₂ gTS⁻¹, that is 33% of that associated to HC_GM_Ext (29.9 mgO₂ gTS⁻¹). This feature could be explained by a possible removal of soluble and biodegradable organic compounds during the preliminary phase of extraction. The hypothesis seems to be confirmed by what observed regarding the germination tests; the greater presence of soluble and biodegradable compounds in HC from non-extracted GM and
the consequent higher consumption of oxygen could have determined a competition effect between
microorganisms and seeds with a prevalence of the former.

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428 3.3 Potential valorization/management of PW

429 3.3.1 Biomethanization Potential of PW

The results of the BMP tests performed on the PW samples are summarized in Figure 6 in terms of 430 431 average cumulative biogas production over time. Methane production started almost immediately in all 432 tests and increased exponentially during the initial phase up to days 12 - 14, albeit at different rates 433 depending on the samples tested. A plateau was reached after about 15 days. The final specific 434 production of methane accounted for 137 and 115 mL CH₄ gCOD⁻¹ for PW GM and PW GM Ext, 435 respectively. These results are comparable to those reported by other authors (Ahmed et al., 2021; 436 Parmar & Ross, 2019) for PW generated from HTC applied to sewage digestate or agricultural waste and fall in the range between 22 and 427 mL CH₄ gCOD⁻¹ indicated by Pagés-Díaz et al. (2020) for HTC liquid 437 438 phase of organic wastes. The average volumetric methane content in the produced biogas was always 439 higher than 40% v/v. The modified Gompertz model matches the BMP experimental results very closely 440 $(R^2 > 0.99)$; the kinetic parameters are reported in Table 5. The process water obtained from HTC of GM 441 and GM_Ext produced methane with a short lag phase of 0.89 - 1.21 days, probably due to the presence 442 of both highly acclimatized microbial consortia and readily degradable organic compounds (Xu et al., 443 2020). This is confirmed also by the obtained values of R_{max} (16.57 – 19.07 mL CH₄ gCOD_i⁻¹ d⁻¹), similar 444 to those obtained by Gaur et al., (2020) for PW generated from HTC applied to sewage sludge. Pagés-Díaz et al. (2020) reported higher values of λ (0.1 - 7.3 mL CH₄ gCOD_i⁻¹ d⁻¹) and lower values of R_{max} 445 446 obtained in similar experimental condition for PW generated from HTC applied to lignocellulosic wastes 447 (6 - 13 mL CH₄ gCOD_i⁻¹ d⁻¹), explained by the formation of some toxic compounds released during the HTC. The lower values of maximum CH₄ production rate and Y_{CH4max} observed for PW_GM_Ext could be 448 449 linked to the already mentioned possible removal of readily available organic compounds during the 450 preliminary extraction treatment.

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453

454 Fig. 6. Cumulative specific biomethane production from the HTC PW versus time and 95% confidence limits (solid455 line indicates Gompertz-model curve).

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Table 5. Kinetic parameters calculated for the BMP tests and associated 95% confidence limits.

Sample		Y _{max} CH ₄ [mL CH ₄ gCOD _i ⁻¹]	R _{max} [mL CH ₄ gCOD _i ⁻¹ d ⁻¹]	λ [d]	R ² [-]
PW_GM	Value	135.71	19.07	1.21	0.998
	Lower 95% conf. limit	132.67	16.64	0.64	
	Upper 95% conf. limit	138.75	21.50	1.78	
PW_GM_Ext	Value	113.86	16.58	0.90	0.996
	Lower 95% conf. limit	110.35	13.86	0.19	
	Upper 95% conf. limit	117.38	19.30	1.61	

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459 3.3.2 Assessment of the potential toxicity of PW in wastewater treatment plants

As autotrophic ammonium-oxidizing bacteria are characterized by slow growth rates and high sensitivity to inhibitors compared to heterotrophs, they can be conveniently employed as test organisms to assess the potential toxicity of liquid streams to be treated in wastewater treatment plants. Moreover, their toxicological responses to several chemicals correlate well to that of *Vibrio fischeri* strain NRRL B11177 and methanogens (Ficara & Rozzi, 2001). The assessments performed in the present study showed potential acute toxicity of PW_GM and PW_GM_Ext at relatively low dosage (the IC₅₀ values were 0.5 and 2.0 mL L⁻¹, respectively) (Figure 7).



Fig. 7. Dose-Response curves showing the acute inhibiting effects of PW_GM and PW_GM_Ext on unacclimated
activated sludge. A sigmoid-function was used to interpolate the experimental data (PW_GM, a=0.58, b= 0.694, R²=
0.944; PW_GM_Ext, a= 3.28, b= 8.547, R²= 0.997).

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Milia et al., (2016b) reported that phenolic compounds might severely inhibit unacclimated activated 473 474 sludge even at low concentrations. Accordingly, the higher inhibiting effect of PW GM is likely due to the 475 expected higher concentration of phenols. As reported in previous studies, liquid streams containing bio-476 recalcitrant compounds with high acute inhibiting effects may be successfully treated using advanced, 477 low-cost, and efficient biological treatment technologies based on self-aggregated biomass such as aerobic granular sludge (Milia et al., 2016a), or well acclimated floc-shaped biomass (Milia et al., 2016b). 478 479 In this sense, the high potential inhibiting effect observed in our study does not necessarily imply that 480 aerobic biological treatment of PW_GM and PW_GM_Ext is not feasible, although particular attention 481 should be paid to biomass selection and acclimation strategies.

482 4. CONCLUSIONS

This work demonstrated the possibility of developing a cascading biorefinery scheme for a multipurpose valorization of grape marc residues. Hydrothermal carbonization, one of the emerging and most 485 promising technologies for the conversion of biomass and wet materials into added-value by-products, 486 represents the core of this biorefinery approach, in which three consecutive processes were considered for their potential integration: a) the recovery of polyphenols by ethanol extraction, b) the production of 487 488 added-value materials and energy through thermochemical conversion, and c) the production of CH₄-rich 489 biogas through anaerobic digestion. The potential for the implementation of HTC in an integrated context 490 of waste biorefinery was addressed by applying the process to both raw grape marc and grape marc 491 previously subjected to polyphenol extraction and recovery treatment. The aerobic treatability of process 492 water was also evaluated in view of its final disposal.

According to the mentioned strategy, the integrated production of bioproducts, soil amendments, peat
substitutes, solid fuels, and biogas was demonstrated.

Compared to the feedstock, the produced hydrochars possess an increased content of fixed carbon and a reduced volatile solids and ash content, as well as an increased HHV and improved quality as a solid fuel, suggesting both the feasibility of using HC as a soil amendment for restoring its organic content and exploiting grape marc by producing energy. The outcomes of the germination tests indicated that HC could be used in low concentration to partially replace peat as a substrate for plant growth. This substitution could shorten the supply chain of soil improvers for Mediterranean grape-producing countries that do not have peat deposits.

The biogas production from PW assessed during the BMP test indicates that energetic valorization through anaerobic biological process may be a feasible option. Over 90% of the output mass from HTC is PW, therefore, this additional option allows for more extensive exploitation of grape marc and the minimization of the potential environmental impact of PW. In contrast, PW showed toxic effects on aerobic microorganisms suggesting that the feasibility of a traditional aerobic treatment must be carefully evaluated.

508 The results obtained and the comparison with what was observed for the process applied to non-extracted 509 GM, although in need of further investigation, seem to suggest that integration can have positive effects 510 in terms of HC quality as soil improver due to the improved biostability and the reduced phytotoxicity.

511

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515

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